

INSTANT SAVING OF ENERGY BILLS AND ELECTRICAL NETWORKS EFFICIENCY IMPROVEMENT

# LV POWER FACTOR CORRECTION SYSTEMS

60Hz FREQUENCY



**GENERAL SALES CONDITIONS** downloadable from our website





#### **ABOUT ORTEA**

# Founded in 1969, ORTEA SpA is a leading company in manufacturing and engineering Power Quality solutions.



Fifty years in the business and ongoing technical research have made of ORTEA SpA a competitive and technologically advanced company.

Close co-operation between design, production and marketing enables to meet the requirements of a constantly growing number of customers.

Beside standard production, ORTEA SpA can be extremely flexible in developing and manufacturing special equipment according to User's specification. All this thanks to the experience gained over many years of applied technological development. Such development includes IT tools that enable the technical staff to elaborate electrical and mechanical designs for each "custom product" on a quick and cost-effective basis.



### QUALITY CERTIFIED





A modern Company that wants to accept the challenge of today's business scenario cannot do so without conforming to standardized organizational criteria.

Customer satisfaction, product quality and responsible occupational practices are the basis on which the Company's activities can be consolidated. ORTEA SpA understood this a long time ago: the first ISO 9001 approval dates back to 1996.

Today ORTEA SpA Integrated Managing System is approved by Lloyd's Register according to the main Standards:

- · ISO9001 (Quality management systems).
- ISO14001 (Environmental management systems).
- OHSAS18001 (Occupational health & safety management systems).

This means that ORTEA SpA can ensure that its performance is optimized in terms of internal process management, commitment towards environmental issues and attention to health & safety at work within the frame of a single Managing System.



## ORTEA POWER QUALITY SOLUTIONS

Companies are more and more sensitive to Power Quality issues because they can cause troubles and damages to equipments and processes, up to interrupting the production cycle.

ORTEA SpA, with his brands ORTEA, ICAR and ENERSOLVE, offers a unique range of products and services for Power Quality and Energy Efficiency of low voltage electrical networks: voltage stabilisers, sag compensator, power factor correction systems, transformers and active harmonic filters.

VOLTAGE VARIATION	VOLTAGE STABILISERS	() ORTEA
SAGs/DIPs	SAG COMPENSATOR	()ORTEA
EXCESSIVE REACTIVE POWER	POWER FACTOR CORRECTION	N SYSTEMS () IEAR
UNPROTECTED LOADS	LV TRANSFORMERS	()ORTEA
HARMONIC POLLUTION	ACTIVE HARMONIC FILTERS	()IEAR
WASTE OF ENERGY	ENERGY EFFICIENCY SMART DEVICES	()ENERSOLVE



# THE 4 REASONS TO HAVE POWER FACTOR CORRECTIONS



**Electricity Authorities.** 

The Electricity Authorities, force companies distributing electricity to apply financial penalties to utilities that have a substantial contractual power and low energy cos phi (generally 0,9). The correct power factor of the electric plant allows you to avoid those penalties, which often are not reflected in the bill, and then are paid by the final user without even realizing it.



Economic convenience.

Economical benefits due to penalties elimination and current reduction, with consequent optimized dimensioning of the components and increased life expectancy.



Energy efficiency.

The power factor correction reduces the "useless" inductive currents required by the loads and that impacts the entire electric network, both in the generation, transmission and distribution stages.

Power factor correction is therefore an important contribution to the energy efficiency of both the user's electrical system and the electricity grid.



Power Quality.

In many industrial electric plants supplied by MT there is a tension considerably distorted, due often to excessive load of MV/LV transformer.

The correct Power Factor Correction with a consequent load reduction by the transformer allow to bring it back to the operating conditions within the linearity limits, substantially reducing the voltage distorsion.

Furthermore the proper Power Factor reduces the presence of harmonic currents.

#### **SERVICES**

It is particularly convenient to install an effective power factor correction system, correctly sized

It is essential to monitor the proper functioning because if you do not keep them in perfect working order, they "lose power", and you are likely to pay penalties.

With proper maintenance you can avoid wasting money and unnecessary power dissipation in the electric plant cables and transformers that undergoes premature aging.

It is also important a proper maintenance and use of original spare parts since capacitors, when worn or of poor quality, are likely to burst causing damage to electrical equipment, plant shutdowns due to protection tripping, or even real fire.

We offer a wide range of services to help you in all situations that must be addressed from the choice of the correct power factor correction system, to commissioning, to management, to replacement.

The measurements can be made with an instrument compliant with IEC 61000-4-30 class A, able to check the energy quality according to the indications of the IEC 50160 standard.



Commissioning.



Design and production according to User's specification.



Design and production for complex plants.



Technical training.



Check-up of existing systems.



Make your own measurement and let us know.



Local support.



**Energy Quality Analysis.** 



Revamping solutions, original spare parts.

#### **GLOSSARY**

#### Cos phi

Simplifying, in an electrical system is appointed with phi  $(\phi)$ , the phase shift between the voltage and the electric current at the fundamental frequency of the system (50Hz). The cos phi is therefore a dimensionless number between 0 and 1, and varies from moment to moment.

Typically, an industrial electrical system has an inductive cos phi, which value depends on the characteristics of the user plant.

#### **Power factor**

In an electrical system means, with power factor, the ratio between the active power and the apparent power. Also the power factor is a dimensionless quantity between 0 and 1, which varies from moment to moment. However, the cos phi and the power factor coincide only in systems devoid of sinusoidal harmonic currents. In a system with harmonic, the power factor is always less than the cos phi.

#### Monthly average power factor

Electricity bills often show the monthly average power factor, obtained from the ratio between the active power consumed by the user and the apparent power transited the point of delivery. Typically, the average monthly power factor is calculated separately on different time slots.

#### **Isolation level**

For a capacitor that complies with IEC 60831-1, the isolation level is indicative of the voltage pulse that can withstand.

#### **Insulation voltage**

For a power factor correction system that complies with the IEC 61439-1/2, the isolation voltage is indicative of the maximum voltage that can withstand the entire system.

#### Nominal voltage of the capacitor U<sub>N</sub>

It is the rated voltage of the capacitor, at which its output rated power is calculated.

#### Maximum operating voltage U<sub>MAX</sub>

It is the maximum voltage that the capacitor can withstand, for the time indicated by the IEC 60831-1/2.

The following relation applies  $U_{MAX} = 1,1 U_{N}$ 

#### Rated operational voltage Ue

It is the rated voltage of the power factor correction system, which guarantees proper use. A capacitor with a rated voltage can have on board capacitors with voltage  $U_{\rm N}$  > Ue. It may never happen otherwise.

#### Short-circuit current lcc

As indicated in the IEC 61439-1, is the prospective short-circuit current that the cabinet can endure for a specified time. It's a value stated by the manufacturer of the cabinet on the basis of laboratory tests. The short-circuit current of the cabinet can be increased, in case of need, by installing fuses. In this case the declared data must be accompanied by the words "fuse conditioning short-circuit current".

#### Resonance

In a LV plant, resonance is the amplification phenomenon of harmonic currents generated by one or more non-linear Loads. The LC circuit is responsible for the amplification, consisting of the MV/LV Power Transformer, that feeds that portion of installation, and by the PF improving capacitor bank. To avoid this phenomenon, wherever there is the risk it might happen, the capacitor bank must be equipped with Harmonic Blocking Reactors.

#### **Steps**

They are the physical units of power factor bank, each controlled by a dedicated switching device (static switch or contactor). A rack may be constituted by a single step (as typically occurs in detuned bank) or more steps. For example, the MULTIrack HP10 from 150kvar/400V consists of 6 steps: 2 from 15kvar and 4 from 30kvar. It 'is easily verified by counting the number of contactors present on the front of the drawer. More step can be merged to achieve larger power steps: in these cases they are controlled by the same controller contact of the reactive power regulator.

#### **Electrical steps**

It is the internal configurations number which proposes a particular automatic power factor corrector, as a function of the steps (number and power) that has on board. For example, a power factor corrector of 280kvar with steps 40-80-160kvar offers 7 combinations: 40-80-120-160-200-240-280kvar. The greater the number of possible combinations, the better "accuracy" and the flexibility to use the power factor correction bank.

#### THD (Total Harmonic Distorsion)

For a periodic non-sinusoidal wave, the THD is the ratio between the rms of all harmonic components value and the rms value of the fundamental at 50Hz/60Hz.

#### **THDI**<sub>c</sub>

It is the maximum THD that a capacitor can withstand, with regard to the current passing through it. It is a characteristic value of each capacitor, indicative of its robustness: much higher is the  $\mathsf{THDI}_{\mathsf{C}}$  more robust is the capacitor.

The THDI<sub>c</sub> is the most significant value to compare different capacitors, together with the maximum temperature of use.

#### THDI<sub>R</sub>

It is the maximum THD bearable by the capacitor relatively to the current that circulates in the plant to be corrected. It is an empirical fact, which is based on the used construction technology and experience of the manufacturer. There is no theoretical link between  $\mathsf{THDI}_R$  and  $\mathsf{THDI}_C$  valid for all plants. The  $\mathsf{THDI}_R$  can also be very different for capacitors with the same  $\mathsf{THDI}_C$  as made by different manufacturers.

#### THDV<sub>R</sub>

It is the maximum voltage THD on the net and also represents the maximum value bearable by a power factor correction bank with harmonic blocking reactors.

#### $f_D$

It is the detuning frequency between inductance and capacitance of a detuned capacitor bank, that is a capacitor bank equipped with harmonic blocking reactors.

The detuning frequency is the most objective parameter for detuned capacitor bank comparison; the lower the detuning frequency is the sounder the capacitor bank is. In particular an 180Hz detuned capacitor bank is sounder and more reliable than another with 189Hz detuning frequency  $f_{\rm D}$ .

As of Ferranti effect, detuned capacitor bank capacitors are exposed to a voltage that is higher than the rated system voltage; for this reason these capacitors are rated for higher voltage compared to the mains voltage.

The according frequency can also be expressed, indirectly, by indicating the detuning factor p%.



# POWER FACTOR CORRECTION: QUALITY AND SAFETY

We define safety the absence of dangers for people and things while the good is in use or stored in a warehouse. This means to identify stresses, risks and potential damages and the relevant elimination and to keep them under control so that to reduce the risk to a reasonable level.

Power capacitors and capacitor banks shall NOT be used:

- For uses other than Power Factor Correction and for AC or DC plants.
- As tuned or detuned filters unless specifically approved in written by ORTEA SpA.

#### **General requirement**

The capacitors are constructed in accordance with IEC - CEI EN methods, parameters and tests. The low voltage capacitors are assembled with the required protection devices and assembled into banks to give a quality product which will operate safely.

They are not considered as the indication that the capacitors and the power factor correction equipments are suitable for a use in the same conditions of the tests. The user has to verify that the capacitor and power factor correction equipment are of the correct voltage and frequency suitable for values of the network on which they are installed. The user has to verify that the installation of the capacitors and/or the power factor correction equipment is in accordance with the catalogue and the instructions of use. Capacitors and power factor correction equipment must not be exposed to damaging action of chemical substance or to attacks of flora and/or fauna.

Capacitors and power factor correction equipments must be protected against risks of mechanical damaging to which could be exposed during normal working conditions or during the installation.

Capacitors and power factor correction equipments that were mechanically or electrically damaged for any reason during the transport, the storage or the installation must not be used and these that breakdown during use must be immediately removed.

# Additional instructions about power factor correction equipments

#### **Definition**

Power factor correction equipment means:

 One or more groups of capacitors that can be connected and disconnected on the network automatically or manually using suitable operating devices (contactors, circuit breakers, load-break switch...).

- · Operating devices.
- · Control, protection and measure systems.
- · Connections.

The equipment could be open or closed inside a metal enclosure.

#### **General requirement**

Follow ORTEA instructions in the documentation attached to equipments considering the safe distance, the connection standard criteria, working standards and the instructions for the controls and the maintenance.

#### Compatibility

It must be paid attention to the electromagnetic interferences with the near by equipments.

#### **Contactors**

It is advisable to adopt capacitor duty contactors (category AC6-b) because they are equipped with pre charge resistors that substantially reduce the inrush currents while capacitors are switched on.

The early switching on of these resistors in respect to the closing or the contactor contacts, allows:

- · To avoid main contacts melting.
- · To avoid capacitor damage.

#### **Recommendations for installation**

#### **Fixing and connection**

To fix the power factor correction equipments it is advised to use these types of screws:

- MICROmatic and MICROfix wall-mounted with Fischer 8.
- MINImatic wall-mounted and floor-mounted with M8 screw.
- MULTImatic and MINImatic floor-mounted with M12 screw.

The installation of the power factor correction equipment is for indoor application; for different use call ORTEA technical department.

#### **Protection devices**

Operating devices (load-break switch) or operation and protection (circuit-breakers if the cables are longer than 3m) must be dimensioned to withstand capacitive currents (about 1.43 times nominal current), the inrush currents, the number of operations and they must be re-strike free.

The capacitors are made of polypropylene that is a flammable material. Even if a fire doesn't begin from capacitors or inside the panel, they could however spread it creating dangerous gasses. If a danger exists from the presence of an explosive or flammable atmosphere, the IEC standard; "Electric equipment with explosion and fire danger", shall be strictly followed.

The protection device must never be opened when the panel is in operation with one or more racks inserted.

#### **Danger for people**

When we install power factor correction equipment we must pay attention that the parts which could be exposed to voltage are correctly protected from accidental contacts in accordance with IEC standards.

Before the commissioning verify the tightening of the terminal and of all the bolts is correct.

#### **Protections**

#### **Overpressure devices**

All the capacitors have an overpressure device which when operated, as in the case of breakdown, disconnects the element from use. This device is not a substitution for the fuses or external circuit-breakers that are specified in our power factor correction equipment.

#### **Limit conditions**

The influence of each factor below has not to be considered individually, but in combination and with the influence of other factors.

#### **Voltage**

Capacitor and capacitor bank nominal voltage is intended as the design and testing voltage.

The safe and proper use of power factor correction capacitors and capacitor banks, implies that the working voltage is not higher than the nominal voltage. In special conditions, excluding the installation phases, higher over voltage are allowed as per below table (ref. IEC 60831).

Overvoltage factor (x U <sub>N</sub> eff)	Max duration	Observation
1	Continuous	Highest average value during any period of capacitor energization. For period less than 24h, exceptions apply as indicated below
1,10	8h every 24h	System voltage regulation and fluctuation
1,15	30 min every 24h	System voltage regulation and fluctuation
1,20	5 min	Voltage rise due to light loads
1,30	1 min	

Note: for voltage without harmonics.

The life expectancy of capacitors and power factor correction equipment is greatly reduced when operating in overload conditions.

The choice of the nominal voltage is determined by the following considerations:

- On some networks working voltage could be very different from nominal voltage.
- · Power factor correction equipment in parallel could cause an increase of the voltage at the connection point.
- The voltage increases with the presence of harmonics on the network and/or cos p of in advance.
- The voltage at the capacitor terminals increases when capacitors are in series with reactors for harmonic blockina.
- If the power factor correction equipment is connected to a motor and not sized correctly, when we disconnect it from the network we may have a phenomena caused by the inertia that makes the motor to work as a self-excited generator consequently increasing of the voltage level at the terminals of the equipment.
- The remaining voltage caused by the self-excited after that the equipment has been disconnected from the network is dangerous for the generators.
- If the power factor correction equipment is connected to a motor with a star-delta starting device we have to pay attention to not cause the overvoltage when this device is working.

· All the power factor correction equipments exposed to overvoltage caused by atmospheric lightning must be protected in correct way.

If surge arresters are used they should be placed as close as possible to the equipment.

#### **Working temperature**

Working temperature of power factor correction equipment is a fundamental parameter for safe operation. As a consequence it is very important that heat generated is dissipated correctly and that the ventilation is such that the heat losses in the capacitors do not exceed the ambient temperature limits.

The highest workings temperature in normal service conditions between two capacitors is measured at a point 2/3 of the capacitors height and at a distance of 1cm from them. The capacitor temperature must not exceed the temperature limits showed in the following table.

	Ambient temperatures [°C]					
		Highest mean over any period of:				
Symbol	Maximum	24h	1 year			
А	40	30	20			
В	45	35	25			
С	50	40	30			
D	55	45	35			

#### **Mechanical Limits**

The user has not to expose the equipment to exaggerated mechanical limits of operation. The user has to pay attention to the electrical and geometrical dimensioning of the connections to avoid exceeding the mechanical limits which may be reached by temperature variation.

#### Other considerations for working safety

#### **Discharge device**

Every capacitor must have a discharge device that can discharge it within 3 minutes.

The discharge time is calculated from the starting peak of voltage equal to rad(2)V<sub>N</sub> until 75V.

Between the capacitor and the discharge system there shall not be a circuit-breaker, fuses or other sectioning devices. This doesn't relief to short-circuit the capacitor terminals and earth every time it is required to handle the capacitor.

#### **Residual voltage**

When the capacitor is placed under tension its residual voltage must not exceed 10% of the rated voltage. This condition is generally satisfied when the power factor correction equipment is calibrated properly, the reactive power controller, reconnection time shall be appropriate to the discharge time.

#### **Enclosure connection**

To keep capacitors enclosure at fix voltage and to discharge fault current toward the case itself, they are grounded by connecting to earth the capacitors supporting frame.

#### **Altitude**

Power factor correction equipment must not be used above an altitude of 2000m. On the contrary please contact technical assistance.

#### **Particular ambient conditions**

Power factor correction equipment are not suitable for the applications in places where there are conditions as follows:

- Fast generation of mould.
- · Caustic and saline atmosphere.
- · Presence of explosive materials or very flammable.
- Vibrations

For environments with these characteristics: high relative humidity, high concentration of dust and atmospheric pollution, please contact technical assistance.

#### **Maintenance**

After the disconnection of the bank, prior to accessing the terminals of the capacitors wait 5 minutes and then shortcircuit the terminals and earth.

Periodically make these procedures:

Once every 6 months:

- Cleanliness by blast of air of the internal part of the power factor correction equipment and of the air filter anytime there is a cooling system.
- · Visual control.
- · Control of the ambient temperature.

#### Once a year:

 Control of the surfaces condition: painting or other treatments.

- Control of the correct tightening of the screw (this operation must be done before the commissioning).
- · Checking the contactors status.
- · Checking the capacitors and chokes (if present) status.

If there are concerns about any environmental conditions an appropriate maintenance program must be established (for example in a dusty environment could be necessary to clean using blasts of air more frequently).

#### Storage and handling

The power factor correction equipment handling must be made carefully avoiding the mechanical stresses and shocks. The equipment in highest cabinet may be hard to handle, because the center of gravity may be very high and decentralized.

Upon receipt of new equipment, make sure that the packaging is not damaged, although mild.

Always make sure that the equipment has not been damaged by transportation: take away the packaging and make a visual inspection with open door. If you discover some damage, write it on the delivery note (carrier copy) the reason for refusal or reserve.

The capacitors and power factor correction awaiting installation storage must be done leaving them in their original packaging, in a covered and dry place.

# **OSTEV** # E



#### **EXPERIENCE**

Founded in 1969, ORTEA SpA has gained experience and know-how that enabled continuous growth and evolution. This never-ending process has allowed the Company to assume a leading role worldwide in designing and manufacturing Power Quality solutions.



#### RELIABILITY

Thanks also to its long-established Quality System, ORTEA SpA can ensure the production of reliable and long lasting products, each one of them accurately tested.



#### **FLEXIBILITY**

In addition to the standard production, the extremely flexible organization of ORTEA SpA is able to develop and manufacture cost-effective special equipment based on the Customer's specification.



#### **QUALITY**

Aiming at providing for the best quality, the manufacturing process includes checks during production and detail test sessions for each equipment. The certified Integrated Managing System ensures the control of every manufacturing phase, starting from checking the components at reception and ending with the best package in relation to the transport type.



# RESEARCH & DEVELOPMENT

ORTEA SpA constantly collaborates with Universities and Business Partners in the research and development of new products and new technologies.



#### **SYNERGY**

By working together, marketing, design, production and after-sales service allow the Company to meet the necessities set forth by an increasingly globalised and competitive market.



#### **EXPERTISE**

ORTEA SpA pre- and after-sales organization is able to intervene quickly, analyzing the problems and providing the correct solution.



#### **CUSTOMER SERVICE**

The continuous monitoring and analysis of requests and claims carried out by the after-sales service enables the improvement the quality of both products and service to the Customer.

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# SIZING AND **SELECTION** CRITERIA

To correctly correct power factor of a LV electrical system we must start from the target we want to achieve.

#### Meaning:

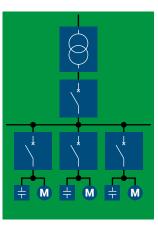
- A higher power factor as measured "at the energy counter" compared to that imposed by the energy authority for excess of reactive energy consumption, so to avoid penalties and / or risk detachment from the network.
- The reduction of currents (and therefore of joules losses and voltage drops) in longer and intensively loaded plant

Depending on the electrical loads features present in the system (working cycle, power, power factor), topology (radial, ring, etc) and the extension of the plant itself, once calculated the power factor correction requirement, it will be clear how to size the capacitor bank.

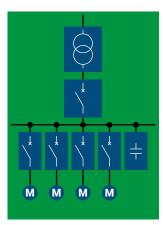
#### LV PFC methods

The most common methods are distributed power factor correction (each of the utilities is equipped with its own unit for power factor correction, typically fixed) and centralized power factor correction (a single automatic PFC system is installed and dedicated to the whole plant).

It is also possible to create "mixed" solutions according to the peculiarity of the plant.



Distributed power factor correction



Centralized power factor correction

#### PF improvement of an asynchronous motor

Typical application of distributed power factor correction is that for a three-phase asynchronous motor. The PFC unit is chosen from tables, remembering to pay attention to the self-excitation risk.

Motor	power	Required reactive power [kvar]				
НР	KW	3000 rpm	1500 rpm	1000 rpm	750 rpm	500 rpm
0,4	0,55	_	_	0,5	0,5	_
1	0,73	0,5	0,5	0,6	0,6	_
2	1,47	0,8	0,8	1	1	_
3	2,21	1	1	1,2	1,6	_
5	3,68	1,6	1,6	2	2,5	_
7	5,15	2	2	2,5	3	_
10	7,36	3	3	4	4	5
15	11	4	5	5	6	6
30	22,1	10	10	10	12	15
50	36,8	15	20	20	25	25
100	73,6	25	30	30	30	40
150	110	30	40	40	50	60
200	147	40	50	50	60	70
250	184	50	60	60	70	80

#### PF improvement of a Power Transformer

In MV electrical systems it is useful to compensate for the reactive power of the MV/LV transformer that supplies the LV part of the system. The required power is worked out starting from the percentage of no-load current (10%). In the absence of this data, the following table can be used.

				<u></u> _
Power	Stan	dard	Low I	osses
transformer [kVA]	Oil [kvar]	Resin [kvar]	Oil [kvar]	Resin [kvar]
10	1	1,5	-	-
20	2	1,7	_	_
50	4	2	-	-
75	5	2,5	_	-
100	5	2,5	1	2
160	7	4	1,5	2,5
200	7,5	5	2	2,5
250	8	7,5	2	3
315	10	7,5	2,5	3,5
400	12,5	8	2,5	4
500	15	10	3	5
630	17,5	12,5	3	6
800	20	15	3,5	6,5
1000	25	17,5	3,5	7
1250	30	20	4	7,5
1600	35	22	4	8
2000	40	25	4,5	8,5
2500	50	35	5	9
3150	60	50	6	10

# CALCULATION OF POWER FACTOR CORRECTION STARTING FROM ENERGY BILL

The calculation of the size of power factor correction required for the system depends on active power (P), from the value of  $\cos \varphi$  that we want to achieve  $(\cos \varphi_2)$ , and from the existing value of  $\cos \varphi$  of the system  $(\cos \varphi_1)$ .

This evaluation can be carried out either from the project data or, for existing plants, from the values shown on the monthly energy bill (for the active power data, refer to the maximum demand active power, or to the contractual active power; or energies consumed in each time band).

In general, the power factor in the F1 and F2 bands is shown on the consumption bill; if not present it can be calculated from the values of active energy Ea and reactive energy Er:

$$\cos \phi_1 = \frac{Ea}{\sqrt{(Ea^2 + Er^2)}}$$

Once the  $\cos \varphi_1$  of the system is known, it should be known which is the target ( $\cos \varphi_2$ ) and according to these two data it is possible to identify in table 1 the coefficient with which to multiply the active contract power, so identifying the necessary reactive power. If there would be a PFC system in the system to be replaced, the reactive power value found must be appropriately increased.

Starting	Target power factor								
power factor	0,90	0,91	0,92	0,93	0,94	0,95	0,96	0,97	
0,67	0,624	0,652	0,682	0,713	0,745	0,779	0,816	0,857	
0,68	0,594	0,623	0,652	0,683	0,715	0,750	0,787	0,828	
0,69	0,565	0,593	0,623	0,654	0,686	0,720	0,757	0,798	
0,70	0,536	0,565	0,594	0,625	0,657	0,692	0,729	0,770	
0,71	0,508	0,536	0,566	0,597	0,629	0,663	0,700	0,741	
0,72	0,480	0,508	0,538	0,569	0,601	0,635	0,672	0,713	
0,73	0,452	0,481	0,510	0,541	0,573	0,608	0,645	0,686	

Extract from Table 1 (See the full table in the APPENDIX).

#### **Example**

System with contractual power: P = 300kW

The Energy bill shows a consumption:

Ea= 32.170kWh Er= 32.652kvarh

We calculate the value of  $\cos \phi_1$ :

$$\cos \phi_1 = \frac{32170}{\sqrt{(32170^2 + 32652^2)}} = 0.7$$

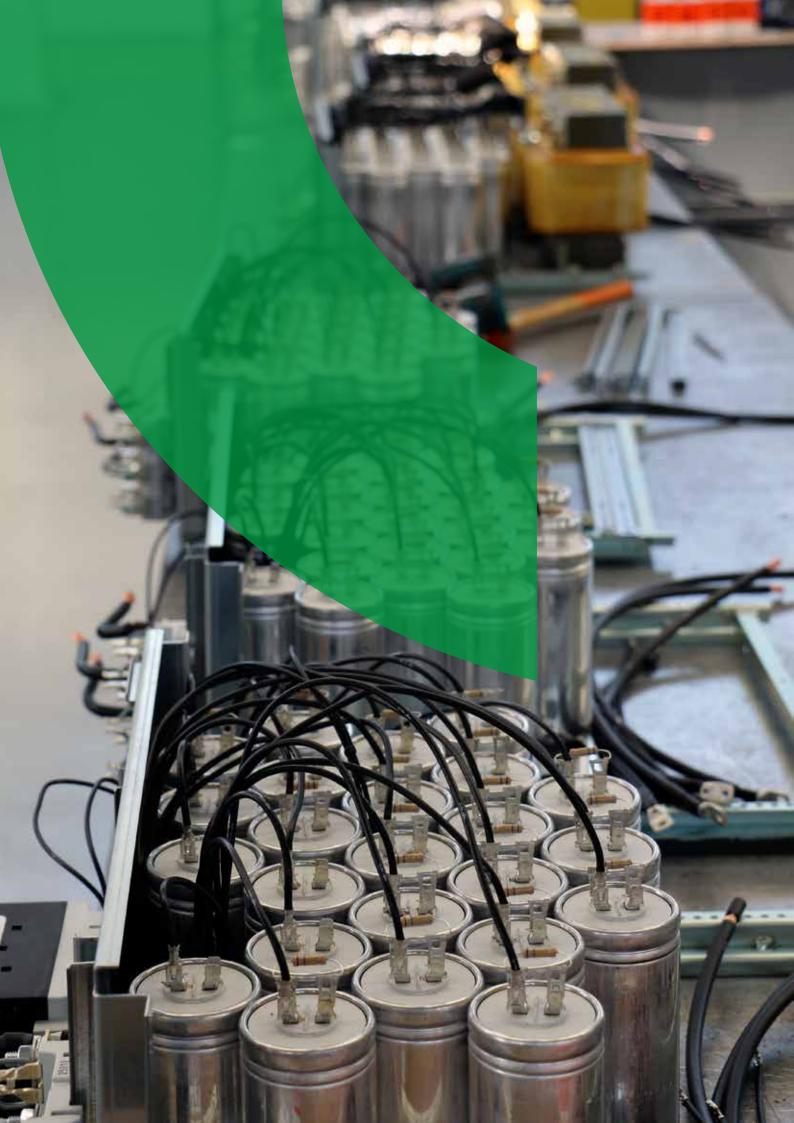
In the table, by choosing 0.70 as the initial power factor and 0.97 as the final power factor, we identify a coefficient equal to 0,77.

The reactive power requirement is therefore equal to:

$$Q_0 = 0.77 * 300 = 231 kvar$$

In the plant there is an old PFC system of 190kvar rated power, but now able to supply 100kvar only (measured with ammeter clamps)

The actual reactive power requirement is therefore equal to 331 kvar.



## CAPACITORS MODELS AND PERFORMANCES WITHIN POWER CORRECTION SOLUTIONS

Once defined the power factor correction required for the plant and the type to be applied (centralized, distributed, mixed), it is a matter of choosing the equipment according to the market offer.

The main element of a power correction system is the capacitor: it is therefore important to choose it strong and of good quality.



#### High gradient metallized polypropylene capacitors



They are dry capacitors made by wrapping a high gradient metallized polypropylene film with metal layer thickness modulated and filled with resin.

The metallization thickness modulation allows to greatly improve the capacitors in terms of:

- Increase in power density (kvar/dm³) with a consequent power size reduction of the power factor correction systems.
- · Robustness improvement against voltage surges, for greater reliability even in systems with the presence of voltage fluctuations due to the network or maneuvers on the system.
- · Improved behavior of the internal short circuit withstand.



#### High gradient metallized polypropylene plus capacitors



They are dry capacitors made by wrapping a high gradient metallized polypropylene film realised with "wavy cut" technology with metal layer thickness modulated and filled with resin. The thickness of the polypropylene film is greater than for standard capacitors. The constructive characteristics allow the operation even at high ambient temperatures, as shown in the table below. They are used in power factor correction systems particularly suitable for heavy duty use.

Main features of the different types of capacitors	High gradient metallized polypropylene capacitors		High gradient metallized polypropylene p capacitors		
Temperature category (IEC 60831-1)*	-25/D			-25/+70 °C	
Max overload	1,3xIn	continuous	1,3xIn	continuous	
Life expectancy at temperature cat25/D	100.000h		150.000h		
Life expectancy at climatic category		100.000h	100.000h		

<sup>\*</sup> Max operating temperature: it is the one measured in the environment surrounding the capacitor

# SOLUTIONS AND COMPONENTS OF AUTOMATIC POWER FACTOR CORRECTION BANKS

In the majority of industrial plants the power factor correction system is centralized, with high capacity capacitor banks usually equipped with harmonic blocking reactors to protect capacitors from harmonics in the current.

When choosing a capacitor bank, it is necessary to pay attention not only to the quality of the capacitors inside the cabinet, but also to the quality of the other components and to the different solutions adopted by the manufacturer, in order to choose a device which will be efficient, long-lasting and easy to maintain.

#### Internal structure

ORTEA SpA manufactures all ICAR APFC with removable rack. It is preferable to choose a capacitor bank with removable racks: it's the best way to reduce time and problems during maintenance.

#### Regulator

It is the intelligent element, which controls the capacitor bank, so it is very important. The regulators on board the ICAR APFC are all microprocessor-based, with several measuring and alarm functions: they will help you understand how the APFC works and how the electrical system to be rephased behaves. You will appreciate it a lot during the capacitor bank's life and in particular when there will be problematic situations.

#### **Contactors**

In order to guarantee excellent long life and reliability, ORTEA SpA ORTEA SpA uses only good well-executed contactors. For standard PFC systems, contactors have to be with damping resistors to limit capacitors inrush current (AC6-b). For detuned PFC systems are enough standard contactors (the function of the peak smoothing It is performed by the blocking reactance).

#### Load break switch

It is the operation element, the one which has to bear the current of the capacitor bank also in case of overload.

According to IEC 60831-1 regulation it has to be dimensioned with a nominal current which is at least 1.43 times the nominal current of the capacitor bank

#### **Steps**

ORTEA SpA manufactures ICAR APFC with a step-by-step that can ensure good accuracy in the correction of the power factor. Typically ICAR realizes its APFC with linear steps, which allows the optimization of the number of electrical combinations obtainable.

#### Harmonic blocking reactors

In detuned APFC, intended for plants with distorted currents and/or resonance risks, the reactors are intended to defend capacitors from harmonic currents, which would damage them. ORTEA SpA designs and builds most of the reactors used in its ICAR APFC, based on the considerable experience gained

#### Ventilation

The ICAR APFC are all made with forced ventilation. This reduces the thermal stress of the on-board capacitors, whether electrically (harmonic overload) and/or ambient (high temperature in the cabin).

#### Filters for the ventilation system

They protect the capacitor bank from the entrance of dust and foreign bodies, which could worsen its thermal situation. During the commissioning, especially if with cable arrival from below, it must be carefully placed so that inbound there are no alternative routes for cooling air: this occurs through the opening of cables passage, if it is not sealed appropriately with ad hoc shaped sets or foams.



#### Fix power factor correction systems



#### **MICROfix**

Power factor correction for fixed three-phase systems, in metal enclosure with IP3X protection degree. MICROfix is equipped with an integrated door lock isolating switch, signal lamps and fuses. For power up to 36kvar at 400V.

#### Automatic power factor correction systems



#### **MICROmatic**

It is the smaller size of automatic power factor correction bank, suitable for small users power factor correction. For reactive power up to 45kvar at 400V in very small dimensions. Allows you to have up to 15 steps for optimal power factor correction in the presence of highly variable loads or characterized by long periods of "no load" operation.



#### **MINImatic**

For small/medium powers automatic power factor correction, can deliver up to 200kvar 400V, depending on the version. It is made with completely removable rack (MINIRack) to simplify management and maintenance.

Very flexible Framework, allows the realization of many variations as shown in the available options table. MINImatic is also available in a version with cable entry from bottom.



#### **MIDImatic**

Automatic power factor correction medium power, can deliver up to 300kvar at 400V depending on the version. It is made with easily removable racks.

It shares many components (including racks) with the mirrored MULTImatic families, for greater robustness and ease of regaining spare parts.

Choice of cable entry (top/bottom).



#### **MULTImatic**

MULTImatic Power factor correction automatic for large users, allows systems of up to several Mvar, with master-slave logic.

MULTImatic is made with rack (MULTIrack) for easy replacement and maintenance.

It is available also in SPEED series (for fast loads), detuned, IP55 (where IP4X wasn't enough), with cable entry from top or bottom.

The distribution of power is with robust aluminium bars (copper on request).

Frameworks of standard equipments made from multiple columns side by side are equipped with a disconnector and a cable entry in each column. Available framework on multiple columns with one single cable entry (consult us).

Note: All fixed and automatic systems must only be mounted in a vertical position.

#### **Automatic Capacitor Banks:**

#### Standard features

These are the common features to all automatic banks: PFC regulator with temperature control, RAL 7035 colour, working voltage Ue of 230V-400V-480V (for different voltage consult us).

	MICRO matic	MINI matic	MIDI matic	MULTI matic
Cable incoming	top/bottom	top	bottom	bottom*
Ventilation	forced	forced	forced	forced
PFC regulator	5LGA	5LGA	8LGA**	8BGA
Degree of protection	IP3X	IP3X	IP3X	IP4X

<sup>\*</sup> MLII TImatic has, in standard, a disconnector and a cable entry for each column. For versions of multiple columns with single cable entry consult us.

#### **Option**

The banks can be made with the following optional equipment: consult us.

	MICRO matic	MINI matic	MIDI matic	MULTI matic
Cable incoming top/bottom	yes	yes (4)	yes (4)	yes (4)
IP55 Degree (cable incoming)	no	yes (bottom)	no	yes
Remote communication (1)	no	no	yes	yes
Control and protection module MCP5	no	no	yes (FH20)	yes (2)
Other paint color (upon request)	yes	yes	yes	yes
Automatic circuit breaker	no	yes (5)	yes	yes
Fuse melting signaling	no	yes	no	yes
Other Short Circuit fault withstand level	no	no	no	yes
Thyristor Switched bank (3)	no	no	no	yes
<b>Controller Remote Software</b>	yes	yes	yes	yes
Fused main Switch	no	yes	yes	yes

<sup>(1)</sup> The regulator can be equipped with additional modules to communicate

#### **Thyristor Switched Capacitor Banks** (speed)

The MULTImatic series can be made with thyristor switches (SPEED version). Compared to traditional power factor correction systems, enables obtaining interesting performances thank to the reaction speed of thyristors, (SCR) that control capacitors banks/steps.

By this solution the following performances are available:

- Switching speed: all the reactive power of the bank can be switched in about 60 ms. This is particularly suitable for plants characterized by fast changing loads (mixers, robots, welders) that could create problems to traditional electromechanic contactors used in standard power factor correction banks.
- Capacitor switching with minimization of the transient current peak. Particularly suitable for plants which power factor correction banks has to perform a great numbers of maneuvers and in presence of devices sensitive to transient over voltage/currents.
- Silence: with no mechanical components on the move, the real time capacitor banks are really suitable for applications where the installation of the power factor correction switchboard occurs near places which require minimum noises (banks, data elaboration centres, theatres, cinemas, libraries, schools, etc).
- Reduced maintenance: the lack of mechanical parts reduces the stress on the switchboard which therefore needs a little periodical maintenance compare to systems with traditional electromechanical contactors. This characteristic is really useful in rooms with conducting powder that could through the conductors into crises.



<sup>\*\*</sup> MIDImatic FH20 is equipped with 8BGA

<sup>(2)</sup> For better protection of power factor correction system against max THD and max Temp. MULTImatic of FH20, FH30, FV40 "detuned" families are equipped in standard with integrated MCP5 in the RPC 8BGA controller.

<sup>(3)</sup> The static switches replace the normal electromechanical contactors and allow the cos φ

djustment even in the presence of loads with sudden changes in absorption

<sup>(4)</sup> To be specified in the order.

# **Power Factor Correction Detuned Filters**

MIDImatic and MULTImatic can be used for perform harmonic filtering. They are banks with reactance connected in series to the capacitors. The LC circuit made in this way, has a network resonant frequency that is different from the network frequency (60Hz) and depending on the electric values of the components used (resistance, capacity, inductance) are obtained different "detuned" filters. These are preferable solutions for those plants characterized by the presence of harmonics due to distorting loads (lighting, power electronics, induction ovens, welders etc), for the reasons described below.

#### **Blocking (detuned) filters**

The detuned filters are designed to power factor correction of a system characterized by the presence of harmonics, "protecting" the capacitors that would be damaged. The addition of the filter does not change the system harmonic content: the harmonics will continue to flow without "enter" into power factor corrector.

The blocking filters have a tuning frequency  $f_{\scriptscriptstyle D}$  lower than that of the harmonic current that circulates in the system with lower order (typically the 5th): a blocking filter is much more robust the lower its tuning frequency. Typically, the tuning frequency  $f_{\scriptscriptstyle D}$  is 216Hz, but in systems with particularly high harmonic content, we realize blocking filters tuned to 162Hz and therefore particularly sound.

The tuning frequency of a barrier filter can also be expressed with other indicators:

- · Order of harmonicity N.
- Barrier factor p (also called "relative impedance" in the IEC 61642 art 2.5), which is usually expressed as a percentage.

Here are the relationships that link these quantities, indicating with f the network frequency,  $X_c$  the capacitive impedance of the capacitors and  $X_t$  the inductive impedance:

$$f_D = \frac{X_L}{X_C}$$
  $N = \frac{f_D}{f}$   $f_D = \frac{f}{\sqrt{D}}$ 

Due to the Ferranti effect, in the detuned systems the voltage which insists on the capacitors ( $U_{\rm c}$ ) is higher than that of the network U according to the following relation:

$$U_c = \frac{U}{1 - p}$$

For this reason the capacitors in detuned systems have to be selected with a suitably high nominal voltage.

# Power factor correction for high voltages systems (> 550V)

The power factor correction systems for applications in nominal voltages of 600/660/690V (eg. voltages used for mining, highway tunnels and rail cargoes on board ship, port cranes, steel mills, paper mills and other "heavy" applications) can be realized in different ways.

#### **Capacitors star connection**

A widely used mode embodiment, but risky, provides a capacitors star connection: in this way capacitors are subjected to a voltage equal to the nominal plant divided by (rad)3.

- Advantages: you can then use capacitors smaller and cheaper, getting more compact and lightweight frameworks.
- Disadvantages: in case the capacity of the capacitors degradations, a phenomenon that is intended, however, to take place, the voltage across the capacitors of the star will no longer be balanced but will increase on the side with greater capacity degrades up to reach values higher than the rated voltage of the capacitors themselves. In this situation, the risk of overvoltage with possible consequent capacitors explosion/fire increases dramatically.

#### Using capacitors at full rated voltage, delta-connected

This solution calls for the use of capacitors with a voltage rating at least equal to that of the network.

- Advantages: equipment electrically robust. Even in case of loss of capacity of a capacitor, the other does not suffer any consequences: you reset the malfunctions risks and capacitors damage.
- Disadvantages: cabinet bulkier and heavier, with higher costs.

#### The ORTEA solution

APFC banks for working voltages higher than 550V are made with delta connected capacitors, and so they have a nominal voltage higher than the system network working voltage; this is the most sound and reliable solution.

To improve power factor of 690V plants, ORTEA SpA uses 900V polypropylene capacitors.

#### Selection criteria depending on the type of plant

The choice of power factor correction equipment must be made by evaluating the design data of the system or, better yet, your electricity bills.

The choice of the power factor correction type must be carried out according to the following table, which shows on the ordinate the rate of harmonic distortion of the plant current (THDI $_{\rm R}$ %) and in abscissa the ratio between the reactive power Q $_{\rm c}$  (kvar) of the PFC bank and LV/MV transformer apparent power  $A_{\tau}$  (kVA).

In light of these data, it identifies the box with proposed families, starting from the family that ensures the proper functioning with the best quality/price ratio.

So you choose the automatic power factor corrector series. The fixed power factor correction must have the same electrical characteristics of the automatic.

The table was made starting from the following assumptions:

- · Network voltage 230V-400V-480V.
- Initial power factor of the plant 0.7 inductive.
- Power factor target 0.95 inductive.
- Non linear load with 5°-7°-11°-13° harmonics current. High frequency harmonics are not allowed.

The hypotheses used are general and valid in the most of cases. In particular situations (harmonics coming from other branch of network, presence of rank equal to or a multiple of 3 harmonics) previous considerations may be invalid. In these cases, the guarantee of a correct choice of the equipment occurs only as a result of a measurement campaign of harmonic analysis of the network and/or the appropriate calculations.

ORTEA SpA disclaims any responsibility for incorrect choice of the product.

#### **PFC systems selection guidelines**

Rated Voltage: 230V	$Q_c / A_T \le 0.05$	$0.05 < Q_{_{\rm C}} / A_{_{\rm T}} \le 0.1$	$0.1 < Q_{_{\rm C}} / A_{_{\rm T}} \le 0.15$	$0.15 < Q_{c} / A_{T} \le 0.2$	$0.2 < Q_{_{\rm C}} / A_{_{\rm T}} \le 0.25$	Q <sub>c</sub> / A <sub>T</sub> > 0,25
THDI <sub>R</sub> % > 27	HP10	FH20	FH20	FH20	FH20	FH20
20 < THDI <sub>R</sub> % ≤ 27	HP10	FH20	FH20	FH20	FH20	FH20
12 < THDI <sub>R</sub> % ≤ 20	HP10	FH20	FH20	HP10	HP10	FH20
THDI <sub>R</sub> % ≤ 12	HP10	HP10	HP10 FH20	HP10	HP10	FH20
Rated Voltage: 400V	$Q_c / A_T \le 0.05$	$0.05 < Q_{c} / A_{T} \le 0.1$	$0.1 < Q_c / A_T \le 0.15$	$0.15 < Q_{c} / A_{T} \le 0.2$	$0.2 < Q_{c} / A_{T} \le 0.25$	Q <sub>c</sub> / A <sub>T</sub> > 0,25
THDI <sub>R</sub> % > 27	HP30	FH20 FH30	FH20 FH30	FH20 FH30	FH20 FH30	FH20 FH30
20 < THDI <sub>R</sub> % ≤ 27	HP30	FH20 FH30	FH20 FH30	HP30	HP30 FH20	FH20 FH30
12 < THDI <sub>R</sub> % ≤ 20	HP30	FH20 FH30	FH20 FH30	HP30	HP30	FH20 FH30
THDI <sub>R</sub> % ≤ 12	HP30	HP30	HP30 FH20	HP30 FH20	HP30	FH20 FH30
Rated Voltage: 480V	$Q_c / A_T \le 0.05$	$0.05 < Q_{_{\rm C}} / A_{_{\rm T}} \le 0.1$	$0.1 < Q_{c} / A_{T} \le 0.15$	$0.15 < Q_{c} / A_{T} \le 0.2$	$0.2 < Q_{c} / A_{T} \le 0.25$	$Q_{c}/A_{\tau} > 0.25$
THDI <sub>R</sub> % > 27	HP30	FV40	FV40	FV40	FV40	FV40
20 < THDI <sub>R</sub> % ≤ 27	HP30	FV40	FV40	FV40	FV40	FV40
12 < THDI <sub>R</sub> % ≤ 20	HP30	FV40	FV40	FV40	FV40	FV40
<b>THDI</b> <sub>R</sub> % ≤ <b>12</b>	HP30	FV40	FV40	HP30 FV40	FV40	FV40

#### Standard power factor correction

The standard power factor correction is used in those plants where there are no current heavily deformed (verify the THD% data of the system current, which must be less than THDI<sub>R</sub>% of the selected power factor correction family) or resonance problems (see the table selection criteria).

If the harmonics presence in the plant is not negligible, are preferred solutions with reinforced capacitors (i.e. with an higher nominal voltage than that of the network).

				FIX		AUTO	MATIC	
	Capacitor construction tecnology	Range and n	ominal values	MICRO fix	MICRO matic	MINI matic	MIDI matic	MULTI matic
<b>=</b>	High gradient metallized polypropylene	HP10*	$THDI_{R} \le 20\%$ $THDI_{C} \le 70\%$ $U_{N} = 415V$	$\checkmark$	$\checkmark$	$\checkmark$		$\checkmark$
	High gradient metallized polypropylene	HP20**	$THDI_{R} \le 20\%$ $THDI_{C} \le 70\%$ $U_{N} = 550V$	✓	$\checkmark$	✓	✓	$\checkmark$
=	High gradient metallized polypropylene	HP30***	$THDIR \le 12\%$ $THDIC \le 50\%$ $U_N = 550V$					$\checkmark$
	High gradient metallized polypropylene plus	VP40***	$THDI_{R} \le 20\%$ $THDI_{C} \le 70\%$ $U_{N} \le 660V$	✓				

<sup>\*</sup> Ue = 230V.

#### Power factor correction with blocking reactors

The power factor correction with blocking reactors (this solution is called in different ways in the technical literature such as "blocking filters", or "detuned filters", or "detuned power factor correctors", etc.) is a solution used when a current flows in the electric system with a high harmonic content (THD) and / or with the resonance risk with the MV/LV transformer.

In these cases, the installation of a "normal" power factor corrector, devoid of blocking reactors, can cause the rapid degradation of the capacitors and cause dangerous electrical and mechanical stresses in the components of power plant (cables, busbars, switches, transformers).

Chokes protect the capacitors by harmonics and at the same time exclude the resonances risk; leave without sacrificing the harmonic content of the current system (if you want to reduce the system harmonic content, you must install active filters. Consult us). This type of power factor correction is therefore to be preferred for systems with important non-linear loads (lighting not luminescent, power electronics, VSD, soft starters, induction furnaces, welding machines...).

ORTEA SpA offers two types of solutions with power factor correction with blocking reactors: one with 216Hz blocking frequency (detuned to 3.6 times the line frequency) and another one with 162Hz (2.7).

It's correct noting that the lower the tuning frequency is the more robust is the cabinet, because the reactor should have a larger iron core.

ORTEA SpA power factor correction solutions with blocking reactor, are made with inductors produced in-house. In addition are used only capacitors with rated voltage higher than that of the network, to ensure strength and durability counteracting the Ferranti effect (permanent overvoltage on the capacitor due to the blocking inductance).

				AUTO	MATIC
	Capacitor construction tecnology	Range and	Range and nominal values		MULTI matic
<b>=</b>	High gradient metallized polypropylene	FH20*	THDI <sub>R</sub> < 100% THDV <sub>R</sub> ≤ 6% $U_N = 550V^{****}$ $f_D = 216Hz (n=3.6)$	✓	✓
	High gradient metallized polypropylene	FH30**	THDI <sub>R</sub> < 100% THDV <sub>R</sub> ≤ 6% U <sub>N</sub> = 550V $f_D$ = 162Hz (n=2,7)		✓
	High gradient metallized polypropylene plus	FV40***	THDI <sub>R</sub> < 100% THDV <sub>R</sub> $\leq$ 6% U <sub>N</sub> = 660V f <sub>D</sub> = 216Hz (n=3,6)		✓

<sup>\*</sup> Ue = 230V / 400V.

<sup>\*\*</sup> Ue = 400V / 480V. \*\*\* Ue = 480V.

<sup>\*\*</sup> Ue = 400V. \*\*\* Ue = 480V.

<sup>\*\*\*\*</sup> At Ue = 230V U<sub>n</sub> = 415V

#### Selection of the CT, its position and how to connect it to the APFC bank

The electronic regulator installed on the capacitor bank calculates the power factor of the plant that has to be corrected by measuring a phase to phase voltage and the related 90° lagging current.

The wiring which is necessary to obtain the signal is realized inside the APFC bank, therefore for a correct operation it is necessary to properly choose, position and wire the CT, which is not included in the capacitor bank.

The CT has to be chosen according to the characteristics of the load that has to be compensated and to the distance between its point of installation and the regulator:

 The primary of the CT has to be chosen according. to the current absorbed by the loads that have to be compensated; it does not depend on the power of the APFC bank. The primary has to be approximately the same (or slightly higher) of the maximum current which can be absorbed by the load. However it is better not to choose a CT with an excessive primary: if this happens, when the load will absorb a limited current the CT will supply to the secondary a current which will be too weak to be calculated by the regulator.

For example, if the load that has to be compensated has a maximum absorption of 90A, it is advisable to choose a CT with a 100A primary.

- The secondary of the CT must be 5A. If you want to use a CT with 1A secondary you will have to parameterize the regulator.
- The performance of the CT (apparent power) must be chosen taking into consideration the dissipation of the cable which connects the CT to the APFC bank. The table below shows how many VA are dissipated for each linear meter of a cable with different sections: to correctly calculate the wiring dissipation you need to consider the total route of the cable (way there and way back).

Cable section [mm²]	VA for each meter of cable at 20°C¹
2,5	0,410
4	0,254
6	0,169
10	0,0975
16	0.0620

1. For each 10°C of temperature variation, the VA absorbed by the cables increase by 4%, the above values are extracted from the typical resistance of flexible class 5 cables

· The precision of the CT is very important to avoid problems of bad functioning of the APFC bank. Choose class 1 CT or, even better, class 0,5.

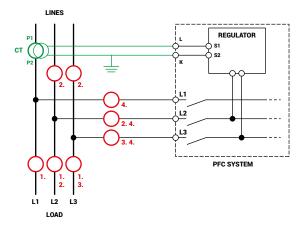
The wiring has to be carried out with an appropriate section. to not excessively weaken the signal coming from the secondary of the CT: choose a 2,5mm<sup>2</sup> cable section only if the wiring between the CT and regulator is 1 m max. Use cable section at least 4mm<sup>2</sup> for wirings up to 10m, 6mm<sup>2</sup> up to 20m and 10 mm<sup>2</sup> for more than 20m wirings (however not recommended).

Connect to earth one of the two clamps of the CT. It is strongly recommended to use a dedicated CT for the APFC bank, to avoid to put in series more than one device (ammeter, multimeter) on the same CT.

#### **Position of the CT**

As before mentioned, the electronic regulator installed on the APFC bank accurately calculates the cosp of the plant if it can measure a phase to phase voltage and the related 90° lagging current.

Since the wiring is already internally carried out on the APFC bank on L2 and L3 phases downstream the load break switch (clamps 9 and 10, see the scheme), the CT must be positioned on phase L1 of the power cable upstream the APFC bank (below image, in green). The side of the CT with P1 (or K) mark has to be oriented to the line (upstream). The wiring of the secondary of the CT (clamps S1 and S2) to the APFC bank (clamps L and K) is made by the customer, according to the instructions in the previous points.



Please note that possible positions here below indicated in red are wrong because:

- 1. the CT is downstream the APFC bank
- 2. the CT is on the wrong phase (L2)
- 3. the CT is on the wrong phase (L3)
- 4. the CT is installed on the cable goes to the APFC bank.

For further information read the regulator's manual.

# Selection of APFC bank protection device

The low Voltage APFC bank equipped with self-healing capacitors are compliant with IEC EN 60831-1/2 (capacitors) and IEC EN 61439-1/2, IEC EN 61921 (complete devices) regulations.

According the above-mentioned regulations, the capacitor bank must be able to work in continuous supporting an rms value of 1.3 times the nominal current (this regulation takes into consideration that, when harmonics are present in the system, capacitors are overloaded).

Known this, and considering that APFC banks can have a tolerance on the nominal reactive power up to 10% more than nominal one, it is possible to indicate the calculation necessary for the choice and setup of the protection device to be installed upstream the APFC bank (Circuit Breaker or Fused Load Break Switch).

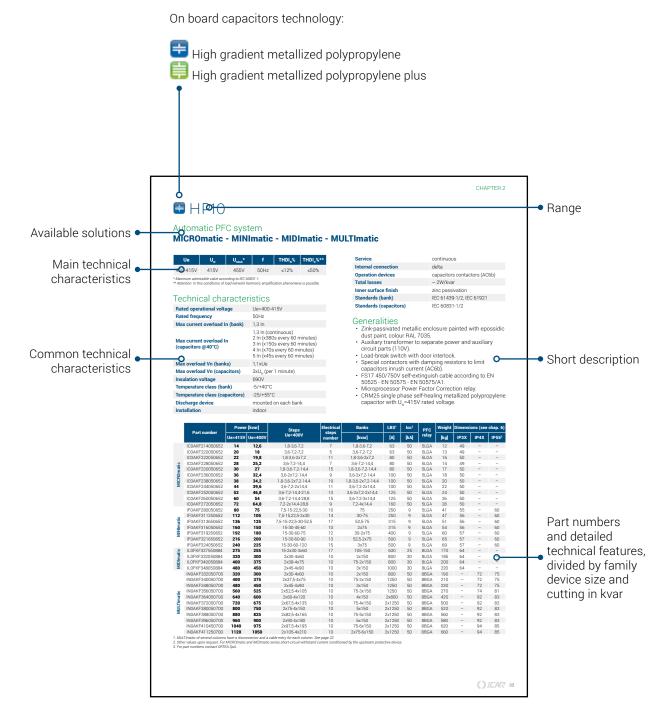
#### **Calculation of the current**

Maximum absorbed current:

$$In_{max} = 1.3 \times 1.1 \times \frac{Qn}{\sqrt{3} \times Vn} = 1.43In$$

Where In is the nominal current of the device calculated with the data present on the label, that is to say Vn (nominal voltage of the network) and Qn (nominal reactive power of the APFC bank at the nominal voltage of the network). It is therefore necessary to choose and install a protection device (Circuit Breaker or Fused Load Break Switch) with current  $\geq$  In  $_{\rm max}$ , value according to which it has to be dimensioned the cable (or bars) which supply the APFC bank.





# POWER FACTOR CORRECTION SOLUTIONS WITH HIGH GRADIENT METALLIZED POLYPROPYLENE CAPACITORS



Range	Fix PFC systems	Automatic PFC systems	Nominal voltage Ue	Capacitors voltage U <sub>N</sub>	THDI <sub>R</sub> %	THDI <sub>c</sub> %	I <sub>250Hz</sub> %	THDV <sub>R</sub> %	f <sub>D</sub>
HP10	✓	$\checkmark$	230V	415V	≤20%	≤70%	_	_	_
HP30	✓	✓	400V	550V	≤20%	≤70%	-	-	_
HP30		✓	480V	550V	≤12%	≤50%	-	-	_
FH20*		✓	230V	415V	100%	-	≤25%	≤6%	216Hz
FH20		✓	400V	550V	100%	-	≤25%	≤6%	216Hz
FH30		✓	400V	550V	100%	-	>25%	≤6%	162Hz

#### Used capacitor

### CRM25-1

- Generalities
  High gradient metallized polypropylene capacitors.
  Metallic case with protection degree IP00.
  Internal overpressure protection system.

  - · Resin filling.

Rated operational voltage	U <sub>N</sub> =415-550V (350-480V)
Rated frequency	50Hz (60Hz)
Max current overload In	1,3xIn (continuous)
Max voltage overload Vn	3xU <sub>N</sub> (for 1 minute)
Temperature class	-25/D
Life expectancy	100.000h
Capacitance tolerance	-5% ÷ +10%
Service	continuous
Construction type	high gradient polypropylene
Standards	IEC 60831-1/2

Range	Part number	Rated voltage U <sub>N</sub> [V]	MAX voltage U <sub>MAX</sub> [V]	Power [kvar]	Capacitance [µF]	Dimensions Ø x h [mm]	Weight [kg]	Pcs/box
	6DCRM00069A50	415	455	0,69	12,2	60x90	0,25	36
LIDIO	6DCRM00138A50	415	455	1,38	25,4	60x90	0,25	36
HP10	6DCRM00275A50	415	455	2,75	50,8	60x140	0,5	36
	6DCRM00550A50	415	455	5,5	101,6	60x140	0,5	36
	6DCRM00069C50	550	600	0,69	7,2	60x90	0,25	36
HP30	6DCRM00138C50	550	600	1,38	14,5	60x90	0,25	36
FH20 FH30	6DCRM00275C50	550	600	2,75	28,9	60x140	0,5	36
	6DCRM00550C50	550	600	5,5	57,9	60x140	0,5	36



#### Fix PFC system

#### **MICROfix**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
230V	415V	455V	60Hz	≤20%	≤70%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- · Load-break switch with door interlock.
- Fuses with high breaking power NH00-gG.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · IP3X protection degree.
- CRM25 single phase self-healing metallized polypropylene capacitor with U<sub>N</sub>=415V-50Hz (350V-60Hz) rated voltage.
- · Discharge resistance.
- · Signal lamp power on.

Rated operational voltage	Ue=230V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Part number	Power [kvar]	LBS	lcc¹	Weight	Dimensions
	Part Humber	Ue=230V	[A] [kA]		[kg]	Difficusions
	IB3DBB160060987	6	40	50	12	43
Ę	IB3DBB180060987	8	40	50	13	43
MICROfix	IB3DBB212060987	12	80	50	15	43
Ī	IB3DBB216060987	16	80	50	18	44
	IB3DBB220060987	20	80	50	20	44

<sup>1.</sup> Other values upon request. Short-circuit withstand current conditioned by the upstream protective device.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.



#### Automatic PFC system

#### **MICROmatic - MINImatic - MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
230V	415V	455V	60Hz	≤20%	≤70%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- Load-break switch with door interlock.
- Special contactors with damping resistors to limit capacitors inrush current (AC6b).
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · Microprocessor Power Factor Correction relay.
- CRM25 single phase self-healing metallized polypropylene capacitor with  $U_N$ =415V-50Hz (350V-60Hz) rated voltage.

Rated operational voltage	Ue=230V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Operation devices	capacitors contactors (AC6b)
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

		Power [kvar]	01	Electrical	Banks	LBS <sup>1</sup>	lcc²	PFC relay	Weight	Dimer	sions
	Part number	Ue=230V	Steps	steps – number	[kvar]	[A]	[kA]		[kg]	IP3X	IP4X
	IC0ABB150060652	5	0,75-1,5-3	7	0,75-1,5-3	63	50	5LGA	12	49	-
	IC0ABB175060652	7.5	1,5-2x3	5	1,5-2x3	63	50	5LGA	13	49	_
	IC0ABB210060652	10	1,5-3-6	7	1,5-3-6	80	50	5LGA	16	50	-
	IC0ABB213060652	13	1,5-2x3-6	9	1,5-2x3-6	80	50	5LGA	14	49	_
Ę	IC0ABB217060652	17	1,5-3-2x6	11	1,5-3-2x6	80	50	5LGA	17	50	-
	IC0ABB220060652	20	1,5-3-6-9	13	1,5-2x3-2x6	100	50	5LGA	18	50	_
	IC0ABB223060652	23	1,5-3-6-12	15	1,5-3-3x6	100	50	5LGA	20	50	-
	IC0ABB227060652	27	3-2x6-12	9	3-4x6	100	50	5LGA	22	50	_
	IF0ABB230060652	30	3-6-9-12	10	30	250	9	5LGA	41	55	-
,	IF0ABB242060652	42	3-6-9-2x12	14	12-30	250	9	5LGA	47	56	_
	IF0ABB251060652	51	3-6-9-12-21	17	21-30	315	9	5LGA	51	56	-
	IF0ABB262060652	62	6-12-18-24	10	2x30	315	9	5LGA	54	56	_
	IF0ABB272060652	72	6-12-24-30	12	12-2x30	400	9	5LGA	60	57	-
•	IF0ABB278060652	78	6-12-24-36	13	21-2x30	500	9	5LGA	65	57	-
	IF0ABB290060652	90	6-12-24-48	15	3x30	500	9	5LGA	69	57	-
	IN0ABB312060700	120	2x12-4x24	10	2x60	800	50	8BGA	190	_	72
	IN0ABB315060700	150	2x15-4x30	10	30-2x60	1250	50	8BGA	210	-	72
	IN0ABB318060700	180	2x18-4x36	10	3x60	1250	50	8BGA	230	_	72
ر	IN0ABB321060700	210	2x21-4x42	10	30-3x60	1250	50	8BGA	270	-	74
MOLIMIAN	IN0ABB324060700	240	2x24-4x48	10	4x60	2x800	50	8BGA	420	_	92
	IN0ABB327060700	270	2x27-4x54	10	30-4x60	2x800	50	8BGA	500	-	92
2	IN0ABB330060700	300	2x30-4x60	10	5x60	2x1250	50	8BGA	520	_	92
-	IN0ABB333060700	330	2x33-4x66	10	30-5x60	2x1250	50	8BGA	560	-	92
	IN0ABB336060700	360	2x36-4x72	10	6x60	2x1250	50	8BGA	580	_	92
	IN0ABB339060700	390	2x39-4x78	10	30-6x60	2x1250	50	8BGA	620	-	94
	IN0ABB342060700	420	2x42-4x84	10	2x30-6x60	2x1250	50	8BGA	660	-	94

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.

<sup>2.</sup> Other values upon request. For MICROmatic series short-circuit withstand current conditioned by the upstream protective device.



#### Fix PFC system

#### **MICROfix**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
400V	550V	600V	60Hz	≤20%	≤70%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- · Load-break switch with door interlock.
- Fuses with high breaking power NH00-gG.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · IP3X protection degree.
- CRM25 single phase self-healing metallized polypropylene capacitor with U<sub>N</sub>=550V-50Hz (480V-60Hz) rated voltage.
- · Discharge resistance.
- · Signal lamp power on.

Rated operational voltage	Ue=400V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (per 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Part number	Power [kvar]	LBS	lcc¹	Weight	Dimensions	
	Part Humber	Ue=400V	[A]	[kA]	[kg]	Difficusions	
	IB3DFF160060987	6	40	50	8	43	
Ę	IB3DFF212060987	12	40	50	9	43	
MICROfix	IB3DFF218060987	18	40	50	12	43	
Ξ	IB3DFF224060987	24	80	50	13	44	
	IB3DFF236060987	36	80	50	15	44	

<sup>1.</sup> Other values upon request. Short-circuit withstand current conditioned by the upstream protective device.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.



#### Automatic PFC system

#### **MICROmatic - MINImatic - MIDImatic - MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
400V	550V	600V	60Hz	≤20%	≤70%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- Load-break switch with door interlock.
- Special contactors with damping resistors to limit capacitors inrush current (AC6b).
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · Microprocessor Power Factor Correction relay.
- CRM25 single phase self-healing metallized polypropylene capacitor with  $U_N = 550V-50Hz$  (480V-60Hz) rated voltage.

Rated operational voltage	Ue=400V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Operation devices	capacitors contactors (AC6b)
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	D	Power [kvar]	Otama	Electrical	Banks	LBS <sup>1</sup>	lcc²	PFC	Weight	Dimer	nsions
	Part number	Ue=400V	Steps	steps number	[kvar]	[A]	[kA]	relay	[kg]	IP3X	IP4X
	IC0TFF190060652	9	1,3-2,5-5	7	1,3-2,5-5	63	50	5LGA	12	49	_
	IC0TFF213060652	13	2,5-2x5	5	2,5-2x5	63	50	5LGA	13	49	_
i i	IC0TFF218060652	18	2,5-5-10	7	2,5-5-10	80	50	5LGA	14	49	-
MICROmatic	IC0TFF223060652	23	2,5-2x5-10	9	2,5-2x5-10	100	50	5LGA	18	50	-
ž.	IC0TFF228060652	28	2,5-5-2x10	11	2,5-5-2x10	100	50	5LGA	22	50	-
₹	IC0TFF233060652	33	2,5-5-10-15	13	2,5-2x5-2x10	125	50	5LGA	24	50	_
	IC0TFF238060652	38	2,5-5-10-20	15	2,5-5-3x10	125	50	5LGA	26	50	-
	IC0TFF245060652	45	5-2x10-20	9	5-4x10	160	50	5LGA	28	50	_
	IC0TFF250060652	50	5-10-15-20	10	50	125	9	5LGA	41	55	-
	IC0TFF270060652	70	5-10-15-2x20	14	20-50	125	9	5LGA	47	56	_
0	IC0TFF285060652	85	5-10-15-20-35	17	35-50	250	9	5LGA	51	56	-
ă	IC0TFF310060652	100	10-20-30-40	10	2x50	250	9	5LGA	54	56	_
2	IC0TFF312060652	120	10-20-40-50	12	20-2x50	250	9	5LGA	60	57	-
MINImatic	IC0TFF313560652	135	10-20-40-65	13	35-2x50	315	9	5LGA	65	57	-
	IC0TFF315060652	150	10-20-40-80	15	3x50	315	9	5LGA	69	57	-
	IC0TFF317060652	170	20-2x40-70	8	20-3x50	400	9	5LGA	78	58	-
	IC0TFF320060652	200	20-40-60-80	10	4x50	400	9	5LGA	88	58	-
	IL1DFF320060884	200	2x20-4x40	10	2x100	400	25	8LGA	230	64	-
matic	IL1DFF325060884	250	2x25-4x50	10	50-2x100	630	25	8LGA	250	64	-
≥	IL1DFF330060884	300	2x30-4x60	10	3x100	800	25	8LGA	280	64	_
	IN2DFF315060700	150	2x15-4x30	10	50-100	400	25	8BGA	230	-	72
	IN2DFF320060700	200	2x20-4x40	10	2x100	400	25	8BGA	252	-	72
	IN2DFF325060700	250	2x25-4x50	10	50-2x100	630	25	8BGA	274	-	72
	IN2DFF330060700	300	2x30-4x60	10	3x100	630	50	8BGA	300	-	72
	IN2DFF335060700	350	2x35-4x70	10	50-3x100	800	50	8BGA	320	-	74
	IN2DFF340060700	400	2x40-4x80	10	4x100	1250	50	8BGA	340	-	74
	IN2DFF345060700	450	2x45-4x90	10	50-4x100	1250	50	8BGA	440	-	70
뜵	IN2DFF350060700	500	2x50-4x100	10	5x100	1250	50	8BGA	480	-	70
E	IN2DFF355060700	550	2x55-4x110	10	50-5x100	2x630	25	8BGA	574	-	92
MULTImatic	IN2DFF360060700	600	2x60-4x120	10	6x100	2x630	50	8BGA	600	-	92
$\leq$	IN2DFF365060700	650	2x65-4x130	10	50-6x100	2x800	50	8BGA	620	-	94
	IN2DFF370060700	700	2x70-4x140	10	7x100	2x1250	50	8BGA	640	-	94
	IN2DFF375060700	750	2x75-4x150	10	50-7x100	2x1250	50	8BGA	660	-	94
	IN2DFF380060700	800	2x80-4x160	10	8x100	2x1250	50	8BGA	680	-	94
	IN2DFF385060700	850	2x85-4x170	10	50-8x100	2x1250	50	8BGA	780	-	93
	IN2DFF390060700	900	2x90-4x180	10	9x100	2x1250	50	8BGA	880	-	93
	IN2DFF395060700	950	2x95-4x190	10	50-9x100	2x1250	50	8BGA	920	-	93
	IN2DFF410060700	1000	2x100-4x200	10	10x100	2x1250	50	8BGA	960	_	93

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.

<sup>2.</sup> Other values upon request. For MICROmatic and MIDImatic series short-circuit withstand current conditioned by the upstream protective device.



#### Automatic PFC system

#### **MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
480V	550V	600V	60Hz	≤12%	≤50%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- · Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- Load-break switch with door interlock.
- · Special contactors with damping resistors to limit capacitors inrush current (AC6b).
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · Microprocessor Power Factor Correction relay.
- CRM25 single phase self-healing metallized polypropylene capacitor with  $U_N = 550V-50Hz$  (480V-60Hz) rated voltage.

Rated operational voltage	Ue=480V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Operation devices	capacitors contactors (AC6b)
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Part number	Power [kvar]	Steps	Electrical	Banks	LBS <sup>1</sup>	lcc²	PFC	Weight	Dimensions
	Part number	Ue=480V		steps number	[kvar]	[A]	[kA]	relay	[kg]	IP4X
	IN2DGG275060700	75	2x7,5-4x15	10	75	250	15	8BGA	145	72
	IN2DGG315060700	150	2x15-4x30	10	150	400	15	8BGA	160	72
	IN2DGG322560700	225	2x23-4x45	10	75-150	400	15	8BGA	175	72
	IN2DGG330060700	300	2x30-4x60	10	2x150	630	28	8BGA	190	72
.0	IN2DGG337560700	375	2x38-4x75	10	75-2x150	800	28	8BGA	210	72
matic	IN2DGG345060700	450	2x45-4x90	10	3x150	800	28	8BGA	230	72
듣	IN2DGG352560700	525	2x53-4x105	10	75-3x150	1250	28	8BGA	270	74
MULTIF	IN2DGG360060700	600	2x60-4x120	10	4x150	2x630	28	8BGA	420	92
2	IN2DGG367560700	675	2x68-4x135	10	75-4x150	2x630	28	8BGA	500	92
	IN2DGG375060700	750	2x75-4x150	10	5x150	2x800	28	8BGA	520	92
	IN2DGG382560700	825	2x83-4x165	10	75-5x150	2x800	28	8BGA	560	92
	IN2DGG390060700	900	2x90-4x180	10	6x150	2x800	28	8BGA	580	92
	IN2DGG397560700	975	2x98-4x195	10	75-6x150	2x1250	28	8BGA	620	94

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.

<sup>2.</sup> Other values upon request.



#### Detuned automatic PFC system

#### **MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	I <sub>250Hz</sub> %**	THDV <sub>R</sub> %	f <sub>D</sub>
230V	415V	455V	60Hz	100%	≤25%	≤6%	216Hz

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- · Load-break switch with door interlock.
- · Contactors for capacitive loads.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · Microprocessor Power Factor Correction relay.
- Control and protection multimeter MCP5, integrated in 8BGA controller.
- CRM25 single phase self-healing metallized polypropylene capacitor with U<sub>N</sub>=415V-50Hz (350V-60Hz) rated voltage.
- Three phase detuning choke with tuning frequency f<sub>n</sub>=216Hz (N=3.6 - p%=7.7%).

Rated operational voltage	Ue=230V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Temperature class (capacitors) Discharge device	-25/+55°C mounted on each bank
,	
Discharge device	mounted on each bank
Discharge device Installation	mounted on each bank indoor
Discharge device Installation Service	mounted on each bank indoor continuous
Discharge device Installation Service Internal connection	mounted on each bank indoor continuous delta
Discharge device Installation Service Internal connection Total losses	mounted on each bank indoor continuous delta ~ 6W/kvar

	Deat work or	Power [kvar]	Steps	Electrical	Banks	LBS <sup>1</sup>	lcc²	PFC	Weight	Dimensions
	Part number	Ue=230V	Ue=400V	steps number	[kvar]	[A]	[kA]	relay	[kg]	IP4X
	IN7ABB288060701	88	12,5-25-50	7	37,5-50	400	25	8BGA	250	72
	IN7ABB313860701	138	12,5-25-2x50	11	37,5-2x50	630	25	8BGA	315	72
	IN7ABB318860701	188	12,5-25-3x50	15	37,5-3x50	800	50	8BGA	380	74
.0	IN7ABB323860701	238	12,5-25-4x50	19	37,5-4x50	1250	50	8BGA	460	70
natic	IN7ABB328860701	288	12,5-25-2x50-100	23	37,5-5x50	1250	50	8BGA	520	71
	IN7ABB335060701	350	2x25-2x50-2x100	14	2x25-6x50	2x800	50	8BGA	740	94
MULTI	IN7ABB340060701	400	2x50-3x100	8	8x50	2x800	50	8BGA	800	94
2	IN7ABB345060701	450	50-4x100	9	9x50	2x1250	50	8BGA	860	90
	IN7ABB350060701	500	2x50-4x100	10	10x50	2x1250	50	8BGA	920	90
	IN7ABB355060701	550	50x5x100	11	11x50	2x1250	50	8BGA	980	91
	IN7ABB360060701	600	2x50-3x100-200	12	12x50	2x1250	50	8BGA	1040	91

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.

<sup>\*\*</sup> Percent current of 5th harmonic.

<sup>2.</sup> Other values upon request.



#### Detuned automatic PFC system

#### **MIDImatic - MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	I <sub>250Hz</sub> %**	THDV <sub>R</sub> %	f <sub>D</sub>
400V	550V	600V	60Hz	100%	≤25%	≤6%	216Hz

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- · Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- · Load-break switch with door interlock.
- · Contactors for capacitive loads.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- Microprocessor Power Factor Correction relay.
- · Control and protection multimeter MCP5, integrated in 8BGA controller.
- CRM25 single phase self-healing metallized polypropylene capacitor with  $U_N = 550V-50Hz$  (480V-60Hz) rated voltage.
- Three phase detuning choke with tuning frequency f<sub>p</sub>=216Hz (N=3.6 - p%=7.7%).

Rated operational voltage	Ue=400V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 6W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

		Power [kvar] Ue=400V	Steps	Electrical steps number	Banks	LBS <sup>1</sup>	lcc² [kA]	PFC relay	Weight [kg]	Dimensions	
	Part number				[kvar]	[A]				IP3X	IP4X
	IL4FFF275060892	75	15-2x30	5	30-45	250	15	8BGA	205	64	-
MIDIMATIC	IL4FFF310560892	105	15-30-60	7	45-60	250	15	8BGA	245	64	_
	IL4FFF313560892	135	15-2x30-60	9	30-45-60	400	20	8BGA	285	64	-
	IL4FFF316560892	165	15-30-2x60	11	45-2x60	400	20	8BGA	300	64	_
	IN7AFF275060701	75	15-2x30	5	30-45	250	17	8BGA	220	-	72
	IN7AFF310560701	105	15-30-60	7	45-60	250	17	8BGA	260	-	72
MOLIIIIauc	IN7AFF313560701	135	15-2x30-60	9	30-45-60	400	25	8BGA	300	-	72
	IN7AFF316560701	165	15-30-2x60	11	45-2x60	400	25	8BGA	325	-	72
	IN7AFF319560701	195	15-2x30-2x60	13	30-45-2x60	400	25	8BGA	365	-	74
	IN7AFF322560701	225	15-30-3x60	15	45-3x60	630	25	8BGA	385	-	74
	IN7AFF325560701	255	15-2x30-3x60	17	30-45-3x60	630	25	8BGA	415	-	70
	IN7AFF328560701	285	15-30-4x60	19	45-4x60	630	25	8BGA	445	-	70
	IN7AFF331560701	315	15-2x30-2x60-120	21	30-45-4x60	800	50	8BGA	475	-	71
	IN7AFF334560701	345	15-30-3x60-120	23	45-5x60	800	50	8BGA	505	-	71
2	IN7AFF337560701	375	15-2x30-60-2x120	25	30-45-5x60	2x400	25	8BGA	775	-	94
	IN7AFF342060701	420	60-3x120	7	7x60	2x630	25	8BGA	800	-	94
	IN7AFF348060701	480	2x60-3x120	8	8x60	2x630	25	8BGA	860	-	94
	IN7AFF354060701	540	60-4x120	9	9x60	2x800	50	8BGA	920	-	90
	IN7AFF360060701	600	2x60-4x120	10	10x60	2x800	50	8BGA	980	-	90
	IN7AFF366060701	660	60-5x120	11	11x60	2x800	50	8BGA	1040	-	91
	IN7AFF372060701	720	2x60-3x120-240	12	12x60	2x800	50	8BGA	1100	-	91

<sup>\*\*</sup> Percent current of 5th harmonic.

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.
2. Other values upon request. For MIDImatic series short-circuit withstand current conditioned by the upstream protective device.



#### Detuned automatic PFC system

#### **MINImatic - MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %   I <sub>250Hz</sub> %**		THDV <sub>R</sub> %	f <sub>D</sub>
400V	550V	600V	60Hz	100%	>25%	≤6%	162Hz

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- · Load-break switch with door interlock.
- · Contactors for capacitive loads.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- Microprocessor Power Factor Correction relay.
- Control and protection multimeter MCP5, integrated in 8BGA controller.
- CRM25 single phase self-healing metallized polypropylene capacitor with  $\rm U_N$ =550V-50Hz (480V-60Hz) rated voltage.
- Three phase detuning choke with tuning frequency f<sub>n</sub>=162Hz (N=2.7 - p%=13.7%).

Rated operational voltage	Ue=400V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+55°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 8W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Power [kvar] Ue=400V	Steps	Electrical steps number	Banks [kvar]	LBS <sup>1</sup>	lcc² [kA]	PFC relay	Weight	Dimensions
Part number								[kg]	IP4X
IN7JFF281060702	81	16-2x33	5	33-49	250	17	8BGA	220	72
IN7JFF311460702	114	16-33-65	7	49-65	250	17	8BGA	260	72
IN7JFF314660702	146	16-2x33-65	9	33-49-65	400	25	8BGA	300	72
IN7JFF317960702	179	16-33-2x65	11	49-2x65	400	25	8BGA	325	72
IN7JFF321160702	211	16-2x33-2x65	13	33-49-2x65	630	25	8BGA	365	74
IN7JFF324460702	244	16-33-3x65	15	49-3x65	630	25	8BGA	385	74
IN7JFF327660702	276	16-2x33-3x65	17	33-49-3x65	630	25	8BGA	415	70
IN7JFF330960702	309	16-33-4x65	19	49-4x65	800	50	8BGA	445	70
IN7JFF334160702	342	16-2x33-2x65-130	21	33-49-4x65	800	50	8BGA	475	71
IN7JFF337460702	374	16-33-3x65-130	23	49-5x65	800	50	8BGA	505	71
IN7JFF340660702	407	16-2x33-65-2x130	25	33-49-5x65	2x630	25	8BGA	775	94
IN7JFF345560702	455	65-3x130	7	7x65	2x630	25	8BGA	800	94
IN7JFF352060702	520	2x65-3x130	8	8x65	2x630	25	8BGA	860	94
IN7JFF358560702	585	65-4x130	9	9x65	2x800	50	8BGA	920	90
IN7JFF365060702	650	2x65-4x130	10	10x65	2x800	50	8BGA	980	90
IN7JFF371560702	715	65-5x130	11	11x65	2x800	50	8BGA	1040	91
IN7JFF378060702	780	2x65-3x130-260	12	12x65	2x800	50	8BGA	1100	91

<sup>1.</sup> MULTImatic of several columns have a disconnector and a cable entry for each column.

<sup>\*\*</sup> Percent current of 5th harmonic

<sup>2.</sup> Other values upon request.

# POWER FACTOR CORRECTION SOLUTIONS WITH HIGH GRADIENT METALLIZED POLYPROPYLENE PLUS CAPACITORS



Range	Fix PFC systems	Automatic PFC systems	Nominal voltage Ue	Capacitors voltage U <sub>N</sub>	THDI <sub>R</sub> %	THDI <sub>c</sub> %	I <sub>300Hz</sub> %	THDV <sub>R</sub> %	f <sub>D</sub>
VP40	✓		480V	660V	≤20%	≤70%	_	_	_
FV40		✓	480V	660V	100%	-	≤25%	≤6%	216Hz

#### Used capacitor

#### CRM25-1

#### Generalities

- High gradient metallized polypropylene capacitors with increased thickness (plus).
- · Metallic case with protection degree IP00.
- · Internal overpressure protection system.
- · Resin filling.



#### Technical characteristics Rated operational voltage U<sub>N</sub>=660V (550V) **Rated frequency** 50Hz (60Hz) 1,3xIn (continuous) Max current overload In Max voltage overload Vn 1.1xU<sub>N</sub> -25/+70°C **Temperature class** Life expectancy 150.000h -5% ÷ +10% Capacitance tolerance Service continuous

Construction type high gradient polypropylene with increased thickness (plus)

Standards IEC 60831-1/2

Range	Part number	Rated voltage U <sub>N</sub> [V]	MAX voltage U <sub>MAX</sub> [V]	Power [kvar]	Capacitance [µF]	Dimensions Ø x h [mm]	Weight [kg]	Pcs/box	
VP40/FV40		660	725	2.65	19.4	60x140	0.5	36	



#### Fix PFC system

#### **MICROfix**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	THDI <sub>c</sub> %**
480V	660V	725V	60Hz	≤20%	≤70%

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### **MICROfix**

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- · Load-break switch with door interlock.
- · Fuses with high breaking power NH00-gG.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · IP3X protection degree.
- CRM25 single phase self-healing metallized polypropylene capacitor with increased thickness and  $U_N$ =660V-50Hz (550V-60Hz) rated voltage.
- Discharge resistance.

#### Technical characteristics

Rated operational voltage	Ue=480V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+70°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 2W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Part number	Power [kvar]	LBS	lcc¹	Weight	Dimensions	
	rai ( liullibei	Ue=480V	[A]	[kA]	[kg]	Dimensions	
×	IB2TGG150060987	5	40	50	14	43	
MICROfix	IB2TGG210060987	10	40	50	15	43	
AIC.	IB2TGG215060987	15	40	50	17	44	
2	IB2TGG220060987	20	80	50	21	44	

<sup>1.</sup> Other values upon request. Short-circuit withstand current conditioned by the upstream protective device.

<sup>\*\*</sup> Attention: in this conditions of load network harmonic amplification phenomena is possible.



#### Detuned automatic PFC system

#### **MULTImatic**

Ue	U <sub>N</sub>	U <sub>MAX</sub> *	f	THDI <sub>R</sub> %	I <sub>250Hz</sub> %**	THDV <sub>R</sub> %	f <sub>D</sub>
480V	660V	725V	60Hz	100%	≤25%	≤6%	216Hz

<sup>\*</sup> Maximum admissible value according to IEC 60831-1.

#### Generalities

- Zink-passivated metallic enclosure painted with epossidic dust paint, colour RAL 7035.
- Auxiliary transformer to separate power and auxiliary circuit parts (110V).
- · Load-break switch with door interlock.
- · Contactors for capacitive loads.
- FS17 450/750V self-extinguish cable according to EN 50525 - EN 50575 - EN 50575/A1.
- · Microprocessor Power Factor Correction relay.
- Control and protection multimeter MCP5, integrated in 8BGA controller.
- CRM25 single phase self-healing metallized polypropylene capacitor with increased thickness and  $\rm U_N$ =660V-50Hz (550V-60Hz) rated voltage.
- Three phase detuning choke with tuning frequency f<sub>n</sub>=216Hz (N=3.6 - p%=7.7%).

#### Technical characteristics

Rated operational voltage	Ue=480V
Rated frequency	60Hz
Max current overload In (bank)	1,3 ln
Max current overload In (capacitors @40°C)	1,3 In (continuous)
Max overload Vn (bank)	1,1xUe
Max overload Vn (capacitors)	3xU <sub>N</sub> (for 1 minute)
Insulation voltage	690V
Temperature class (bank)	-5/+40°C
Temperature class (capacitors)	-25/+70°C
Discharge device	mounted on each bank
Installation	indoor
Service	continuous
Internal connection	delta
Total losses	~ 6W/kvar
Inner surface finish	zinc passivation
Standards (bank)	IEC 61439-1/2, IEC 61921
Standards (capacitors)	IEC 60831-1/2

	Don't word on	Power [kvar]	04	Electrical	Banks	LBS <sup>1</sup>	lcc²	PFC	Weight	Dimensions
	Part number	Ue=480V	Steps	Steps steps number	[kvar]	[A]	[kA]	relay	[kg]	IP4X
	IN5TGG311060701	110	22-2x44	5	22-2x44	250	15	8BGA	315	72
	IN5TGG315460701	154	22-3x44	7	22-3x44	400	15	8BGA	380	74
	IN5TGG319860701	198	22-4x44	9	22-4x44	400	15	8BGA	460	70
	IN5TGG324260701	242	22-5x44	11	22-5x44	630	28	8BGA	520	71
Ę.	IN5TGG326460701	264	6x44	6	6x44	630	28	8BGA	580	71
Imatic	IN5TGG330860701	308	2x22-2x44-2x88	14	2x22-6x44	2x400	15	8BGA	740	94
MULTI	IN5TGG333060701	330	22-3x44-2x88	15	22-7x44	2x400	15	8BGA	770	94
₹	IN5TGG335260701	352	2x44-3x88	8	8x44	2x400	15	8BGA	800	94
	IN5TGG339660701	396	44-4x88	9	9x44	2x630	28	8BGA	860	90
	IN5TGG344060701	440	2x44-4x88	10	10x44	2x630	28	8BGA	920	90
	IN5TGG348460701	484	44-5x88	11	11x44	2x630	28	8BGA	980	91
	IN5TGG352860701	528	2x44-3x88-176	12	12x44	2x630	28	8BGA	1040	91

MULTImatic of several columns have a disconnector and a cable entry for each column.
 Otherwolves upon request.

<sup>\*\*</sup> Percent current of 5th harmonic.

<sup>2.</sup> Other values upon request.



**RPC 5LGA** 



**BPC 8LGA** 



**RPC 8BGA** 

# REACTIVE POWER REGULATOR

The reactive power regulator is, together with the capacitors and reactors (in detuned filter cabinets), the key component of the automatic power factor correction system.

It is in fact the "intelligent" element, responsible for the verification of the power factor of the load, in function of which controls the switching on and off of the capacitors batteries in order to maintain the power factor of the system beyond the target.

The reactive power regulators RPC used in ICAR branded automatic power factor correction systems are designed to provide the desired power factor while minimizing the wearing on the banks of capacitors, accurate and reliable in measuring and control functions are simple and intuitive in installation and consultation.

By purchasing a branded ICAR automatic power factor correction system you receive it ready for commissioning. In fact the controller is already set, you just need to connect it to the line CT and set the value of the primary current. The controller automatically recognizes the current direction of the CT secondary, to correct any wiring errors.

The flexibility of regulators allows you to modify all the parameters to customize its operation to fit the actual characteristics of the system to be corrected (threshold power factor, sensitivity of step switching, reconnecting time of the steps, presence of photovoltaics, etc.).

As described below, the regulators offer important features as for the maintenance and management of the power factor correction bank, aimed at identifying and solving problems, which could lead to its damage with consequent life expectancy reduction.

System	Regulator
MICROmatic	RPC 5LGA
MINImatic	RPC 5LGA
MIDImatic	RPC 8LGA
MIDImatic (with detuning reactor)	RPC 8BGA + MCP5
MULTImatic	RPC 8BGA + MCP5 (optional)
MULTImatic (with detuning reactor)	RPC 8BGA + MCP5

#### Reactive power regulators RPC 5LGA and RPC 8LGA

RPC 5LGA

Selection keys, parameters editing and confirmation

Communication optical port USB-WIFI

The reactive power regulator RPC 5LGA equips MICROmatic and MINImatic automatic power factor correction systems, while the new regulator RPC 8LGA equips MIDImatic. Both are managed by a microprocessor and offer many features maintaining a simple user interface locally or from a PC

They are characterized by a large LCD display with text messages (in 6 languages: ITA, ENG, FRA, SPA, POR, GER) and icons for quick and intuitive navigation.

The regulators are very flexible: they are in fact able to adjust the power factor between 0.5 inductive and 0.5 capacitive, to operating with power from 100 to 440 VAC, to run on the 4 quadrants for cogeneration installations, to accept in Input CT secondary 5A or 1A.

The regulators have standard temperature control and the ability to configure one of the available relays for activating visual alarms sound at a distance; also control the distortion of current and voltage.

Regulators RPC 5LGA-8LGA can operate in automatic or manual mode: in the first case in complete autonomy by switching batteries available up to the desired power factor; in the second case it will be the operator to force the insertion and disconnection of the battery: the regulator still oversee operations to prevent potential damage to the capacitors (for example by assessing compliance of discharge times before a subsequent insertion).

#### **Measurement functions**

Regulators RPC 5LGA and 8LGA provide many standard measurements in order to check and monitor the correct electrical and temperature conditions of the power factor correction system.

Display shows the following values: power factor, voltage, current, delta kvar (reactive power missing to reach the target power factor), average weekly power factor, total harmonic distortion of the current system (THDI $_{\rm R}$ %) with detailed harmonic for harmonic from 2nd to 15th, total harmonic distortion of the voltage (THDV $_{\rm R}$ %) with detail for harmonic harmonic from 2nd to 15th, total harmonic distortion in the current % (THDI $_{\rm C}$ %) capacitor, temperature.

The controller stores and makes available for consultation the maximum value of each of these variables, to evaluate the most severe stress suffered by the automatic power factor correction since the last reset: the temperature, the voltage and the total harmonic distortion have a strong impact on the capacitors as if they hold more than the nominal values can drastically reduce the service life.

#### Alarmo

The ICAR RPC regulators offer many different alarms as standard, which help in the correct operation of the system. The alarms are set to the following values:

- Under-compensation: the alarm is activated if, with all the steps of power factor correction switched on, the power factor is lower than the desired value.
- Over-compensation: the alarm is activated if, with all the steps of power factor correction switched off, the power

factor is greater than the desired value.

- Minimum and maximum current: to assess the condition of the system load.
- Minimum and maximum voltage: to evaluate the stresses due to the variations of the supply voltage.
- Maximum THD%: to assess the pollution of network as regards to harmonic current.
- Maximum temperature in the enclosure: to monitor the capacitor climatic conditions.
- Short voltage interruptions.

Alarms are programmable (enable, threshold, time of activation / deactivation).

#### **Display Indications**

The LCD display icons and text provides the following information for quick identification of the state of the system:

- · Operating mode automatic/manual.
- Status of each battery (on / off).
- · Recognition power factor inductive / capacitive.
- Type of value displayed.
- Active alarm code, and explanatory text (in a language of choice among the 6 available: ITA, ENG, FRA, SPA, POR, GFR)

#### Safety

The RPC 5LGA and 8LGA controllers have passwords to prevent not authorized access.

A backup copy of the factory settings is always available in memory.

#### **Contacts**

The regulators RPC 5LGA and 8LGA have power contacts for controlling the steps, to control the eventual cooling fan and for the activation of alarms to distance; contacts are NO and have a range of 5A at 250Vac or 1.5A at 440Vac.

A contact is in exchange for alarm functions (NO or NC).

#### **Additional module**

The regulator RPC 5LGA has the ability to accommodate, in the back slot, an additional module.

The regulator RPC 8LGA has two rear slots to accommodate up to two additional modules.

Once installed an additional module, the controller recognizes and activates the menu for its programming.

Additional modules can be installed even in the bank already in service. Slots for additional module may be already used to implement necessary functions to the context in which the controller is mounted. If you decide to add a module to an already operating, ensure that there is an available slot.

- **OUT2NO** two digital outputs module for additional step control (two 5A 250Vac relays)
- COM232 isolated RS232 interface
- COM485 isolated RS485 interface
- WEBETH Ethernet interface (only for RPC 8LGA)



Data sheet	RPC 5LGA	RPC 8LGA		
Control	microp	rocessor		
Auxiliary supply voltage	100÷440Vac			
Frequency	50Hz	z/60Hz		
Voltage measuring input	100-	÷600V		
Current measuring input	5A (1A pro	grammable)		
Current reading range	from 25mA to 6A (	(from 25mA to 1.2A)		
Automatic current way sensing	yes			
Operation in systems with cogeneration	yes			
Power consumption	9.5VA			
Output relay	5A - 250Vac			
Cosφ adjustment	from 0.5 in	d. to 0.5 cap.		
Step switching time	1s ÷	1000s		
Alarm relay	У	res		
Degree of protection	IP54 on front, I	P20 at terminals		
Operating temperature	from -20°	C to +60°C		
Storage temperature	from -30°	C to + 80°C		
Front optical port		on USB or WIFI with accessories		
Compliance with the standards		00-6-2; IEC 61000-6-4; A C22-2 nr.14		
Output relay number	5 (expandable up to 7)	8 (expandable up to 12)		
Dimensions	96x96mm	144x144mm		
Weight	0.35kg	0.65kg		
Part number	6CF46411050	6CF025		

#### **Reactive power regulators RPC 8BGA**



The RPC 8BGA reactive power regulator equips MULTImatic automatic power factor correction systems. It is a very innovative controller, with exclusive features:

- · High electrical performance
- · Extended Capabilities
- · Graphic display
- Advanced communication
- · Upgradability, even after installation
- · Powerful supervision software
- · Choice language (10 languages available on board).

More details below, referring to the following page tables and manuals for further information.

#### **High electrical performance**

The 8BGA controller is equipped with powerful hardware, which allows a considerable electrical performances: it can be connected to the CT secondary 5A or 1A, it can work on networks with voltages from 100 to 600Vac with a measuring range from 75Vac to 760Vac, it can be connected to a single CT (typical configuration of the power factor corr ection) or three-CTs (for a more accurate measurement of the power factor, and this fact makes the 8BGA controller to refocus and to be a multimeter as well).

#### **Extended Capabilities**

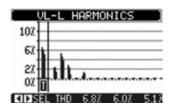
The 8BGA reactive power regulator is controlled by a powerful microprocessor that allows a set of new functions to solve problems even in complex plant.

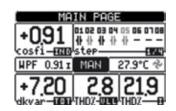
8BGA can work master-slave functions, handles up to 10 languages simultaneously, can be used in MV systems managing the transformation ratio of the VT, it can support multiple inputs and outputs via optional modules, it can handle target cos phi from 0.5 inductive to 0.5 capacitive. 8BGA can build a network of 4 wired units (one master three slaves) to be able to handle up to 32 steps of power factor correction in a consistent and uniform way.

#### Graphical display with high readability

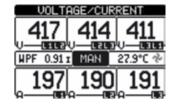
Forget the regulators with small displays and difficult to read: 8BGA will amaze you with its display matrix graphic LCD 128x80 pixels.

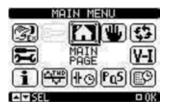
The detail and sharpness allow intuitive navigation between the different menus, represented with text and icons.













#### **Advanced communication**

8BGA born to be a regulator able to communicate in a manner in line with the latest technology: Ethernet, RS485, USB, WIFI.

Now you can see the information of the company cos phi, without having to go in front of the regulator. Now you can consult it by a PC.

The information about the cos phi is important, because it impacts heavily on the company's income statement.

#### **Evolutivity**

The "basic" 8BGA regulator can be enhanched with up to four additional modules "plug and play" which greatly expands its performance.

It is possible to add additional control relays (up to a total of 16), even for a static control (thyristors), digital and analog inputs, analog outputs, communication modules.

Your controller can become a small PLC, and the PFC system can become a point of data aggregation, for remote communication.

#### Measurement functions and help to maintain

8BGA is a real evolved multimeter, thanks also to the graphic display of excellent readability and to the powerful microprocessor.

The measured parameters are the basic ones ( $\cos \varphi$ , PF, V, I, P, Q, A, Ea, Er) with the addition of the distortion of the voltage and current (THD, histogram of the value of each harmonic, waveform graphic visualization).

If 8BGA is connected to three CT, the harmonic analysis is detailed for each phase, in order to identify any anomalies of single phase loads. 8BGA measure and count values that can help in ruling the PFC (temperature, number of switching of each step). 8BGA also suggests the maintenance to be carried out by means of simple messages on the display. Keep efficient capacitor becomes much easier.

8BGA stores the maximum values of current, voltage, temperature, each associated with the date and time of the event for a better analysis of what happened.

#### **Alarms**

The set of alarms (maximum and minimum voltage, maximum and minimum current, over and undercompensation, overload of the capacitors, maximum temperature, microinterruption) associated with the readability of the messages on the display allows a better understanding of what happened.

Even alarm programming (enable / disable, delay, relapse etc.) is easier and faster.

Data sheet	RPC 8BGA				
Controllo	a microprocessore				
Auxiliary supply voltage	100÷440Vac				
Frequency	50Hz/60Hz				
Voltage measuring input	100÷600V (-15% / +10%)				
Current measuring input	5A (1A programmable)				
<b>Current reading range</b>	from 25mA to 6A (from 10mA to 1.2A)				
Automatic current way sensing	yes				
Operation in systems with cogeneration	yes				
Power consumption	12VA (10.5W)				
Output relay	5A - 250Vac				
Cosφ adjustment	from 0.5 ind. to 0.5 cap. (tan φ da -1.732 a +1.732)				
Step switching time	1s ÷ 1000s (20ms with STR4NO module)				
Alarm relay	yes				
Degree of protection	IP55 on front, IP20 at terminals				
Operating temperature	from -30°C to +70°C				
Storage temperature	from -30°C to +80°C				
Front optical port	for communication USB or WIFI with dedicated accessories				
Temperature control	from -30°C to +85°C				
Compliance with the standards	IEC 61010-1; IEC 61000-6-2; IEC 61000-6-3; UL508; CSA C22-2 nr.14				
Output relay number	8 (expandable up to 16)				
Dimensions	144x144mm				
Weight	0.98kg				
Part number	6CF46411000				

#### Additional modules

The RPC 8BGA controller accommodates up to 4 additional modules "plug & play". Once you have added an additional module, the controller recognizes and activates the menu for its programming. Additional modules can also be installed retrospectively (consult us).

#### **Digital inputs and outputs**

These modules allow you to increase the contacts funding for control of the steps contactors (OUT2NO module) or thyristors (STR4NO module) switched banks, or to add inputs and / or digital / analog acquisition of parameters and implementing simple logic.

- OUT2NO module 2 digital outputs to control additional steps (two relays 5A 250 Vac)
- STR4NO module 4 static outputs for thyristor control steps (range SPEED)
- INP40C module 4 digital inputs

#### **Protection functions**

The control and protection module MCP5 allows a more detailed inspection of the electrical parameter and temperature that can damage the capacitors. Thanks to algorithms particularly suitable for automatic equipment consisting of capacitors and reactors.

 MCP5 module for protection and control for additional safety of capacitors, especially suitable in the detuned banks

MULTImatic detuned systems are equipped with RPC 8BGA controller with MCP5 module.

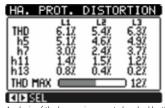
This module has very important function: it directly monitors, through two CTs installed inside, the current in the capacitors analyzing the harmonic content.

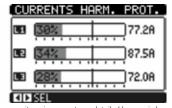
In case of harmonic content increases (for example, due to the aging of the capacitors) exceeding a certain limit value, the PFC system is taken out of service, excluding the risk of bursting or overcharging of the capacitors.

The MCP5 module allows the harmonic currents affecting the capacitors to be monitored directly on the RPC 8BGA controller screens, as can be seen in the two pictures shown below.

The individual harmonics are kept under control, with the possibility of setting an alarm level and an intervention level on each. The MCP5 module also allows to monitor two additional temperatures in order to avoid excessive overheating even inside the panel.

Without this functionality, the regulator would carry out the evaluation of the harmonic content with greater difficulty and less precision.





Analysis of the harmonic current absorbed by the capacitors, in percentage, detailed harmonic by harmonic, and absolute.

#### **Communication functions**

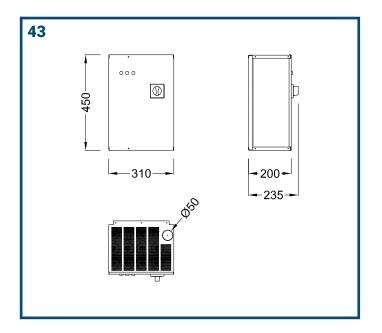
RPC 8BGA regulator is very powerful in terms of communication. The modules dedicated to these functions allow multiple solutions to remotely control the power factor system and all other variables measured, calculated or obtained from the instrument.

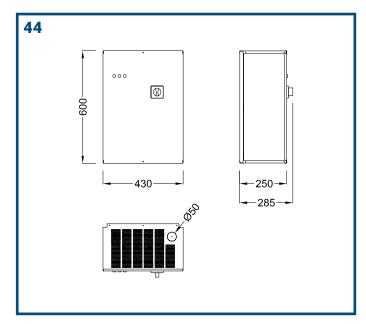
- COM232 isolated RS232 interface
- COM485 isolated RS485 interface
- WEBETH Ethernet interface
- COMPRO isolated Profibus-DP interface
- CX01 cable connection from the RPC 8BGA optical port to the USB port of the computer for programming, downloading / uploading data, diagnostics etc
- **CX02** device to connect the optical port in the RPC 8BGA via WIFI: for programming, downloading / uploading data, diagnostics etc

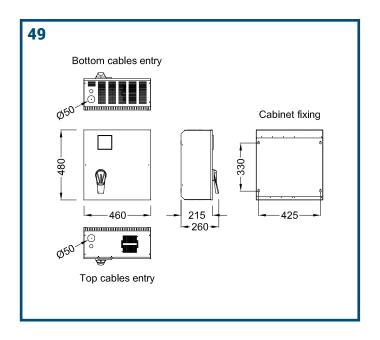
### DIMENSIONS

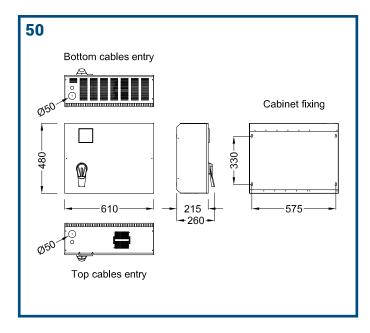
The following pages show the dimensions of the equipment in this catalog, identified with the respective numerical code. This page shows the total dimensions, for a first evaluation of the space occupied. The dimensions in the table include (where present) handles, exchangers, turrets, etc. For more details, consult the individual drawings.

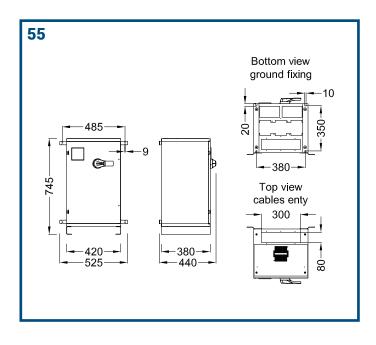
	dimensional	Dir	mensions [m	ım]
	number	w	D	Н
MICROfix	43	310	200	450
	44	430	250	600
MICROmatic	49	460	260	480
	50	610	260	480
MINImatic	55	420	425	745
	56	420	425	965
	57	420	425	1183
	58	420	425	1403
MIDImatic	64	600	690	1835
MULTImatic	70	610	670	2160
	71	610	670	2360
	72	610	670	1760
	74	610	670	1960
	90	1220	670	2160
	91	1220	670	2360
	92	1220	670	1760
	93	1220	777	2160
	94	1220	670	1960

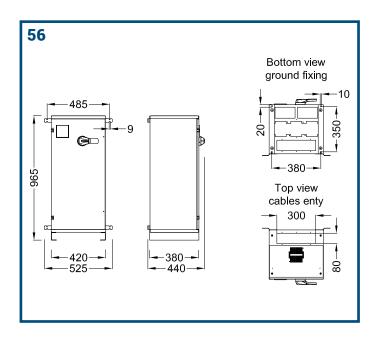


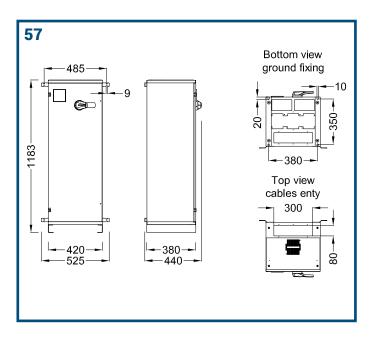


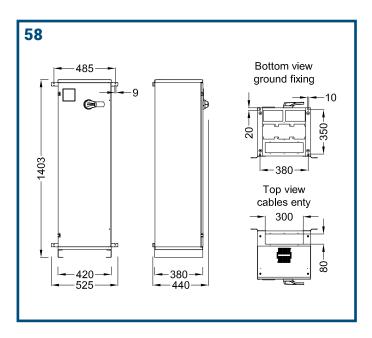


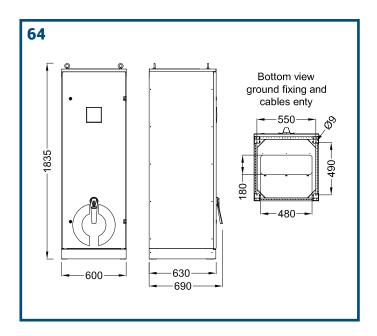


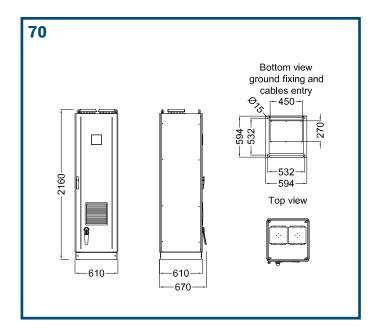


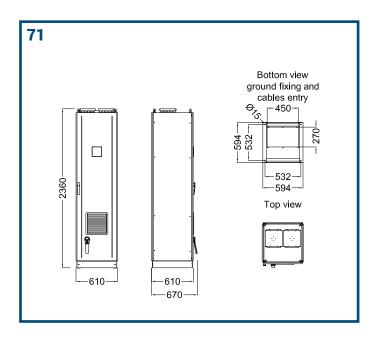


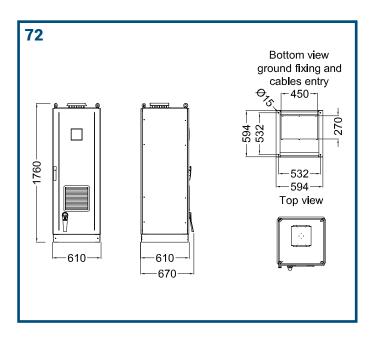


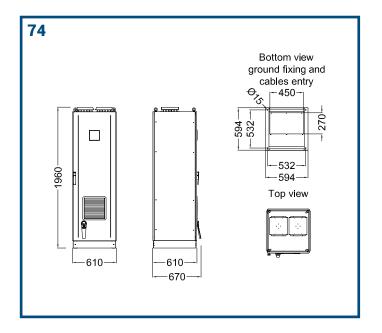


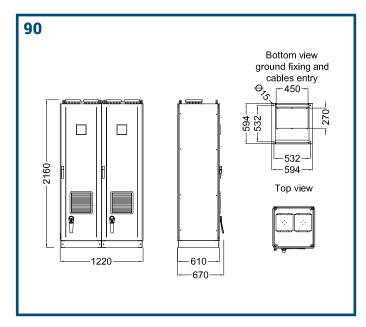


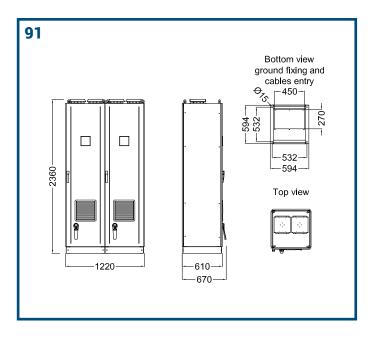


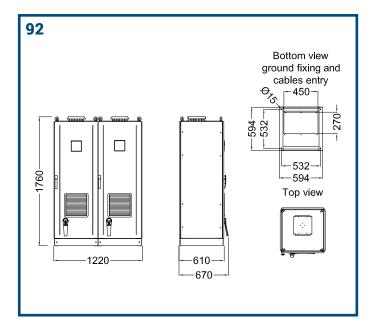


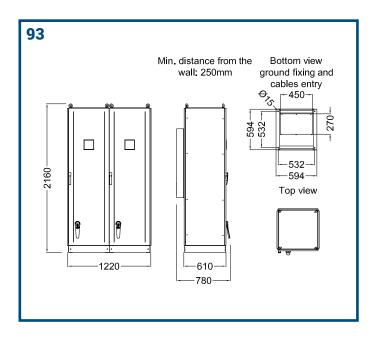


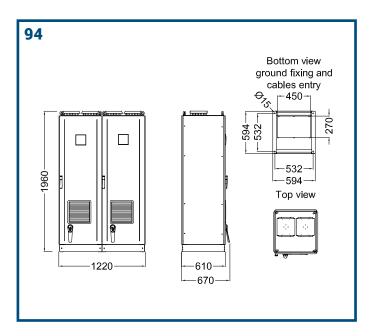








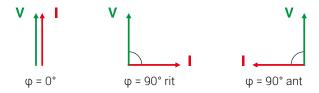




#### TECHNICAL NOTES

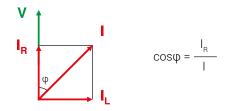
#### Power factor correction: why?

In electrical circuits the current is in phase with the voltage whenever are in presence of resistors, whereas the current is lagging if the load is inductive (motors, transformers with no load conditions), and leading if the load is capacitive (capacitors).



The total absorbed current, for example, by a motor is determined by vector addition of:

- I<sub>R</sub> resistive current;
- I inductive reactive current;



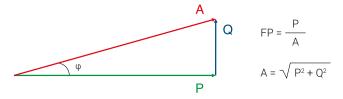
These currents are related to the following powers:

- Active power linked to I<sub>p</sub>;
- Reactive power linked to I,;

The reactive power doesn't produce mechanical work and it is an additional load for the energy supplier.

The parameter that defines the consumption of reactive power is the power factor.

We define power factor the ratio between active power and apparent power:



As far as there are not harmonic currents power factor coincides to cosφ of the angle between current and voltage vectors

Cosp decreases as the reactive absorbed power increases.

Low cosφ, has the following disadvantages:

- High power losses in the electrical lines.
- · High voltage drop in the electrical lines.
- · Over sizing of generators, electric lines and transformers.

From this we understand the importance to improve (increase) the power factor.

Capacitors need to obtain this result.

#### Power factor correction: how?

By installing a capacitor bank it is possible to reduce the reactive power absorbed by the inductive loads in the system and consequently to improve power factor. It is suitable to have  $\cos\varphi$  a little in excess of 0.95 to avoid paying the penalties provided for by the law.

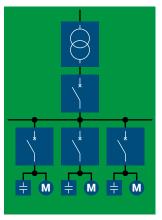
The choice of the correct power factor correction equipment depends on the type of loads present and by their way of working.

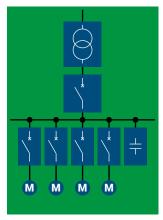
The choice is between **individual compensation** and **central compensation**.

Nel caso di rifasamento distribuito, le unità rifasanti sono disposte nelle immediate vicinanze di ogni singolo carico che si vuole rifasare.

Individual compensation: power factor correction is wired at each single load (i.e. motor terminals).

Central compensation: there is only one bank of capacitors on the main power distribution switch board or substation.





Individual compensation

Central compensation

The individual compensation is a simple technical solution: the capacitor and the user equipment follow the same sorts during the daily work, so the regulation of the  $\cos \phi$  becomes systematic and closely linked to the load. Another great advantage of this type of power factor correction is the simple installation with low costs.

The daily trend of the loads has a fundamental importance for the choice of most suitable power factor correction. In many systems, not all the loads work in the same time and some of them work only a few hours per day. It is clear that the solution of the individual compensation becomes too expensive for the high number of capacitors that have to be installed. Most of these capacitors will not be used for long period of time.

The individual compensation is more effective if the majority of the reactive power is concentrated on a few substatios loads that work long period of time.

Central compensation is best suited for systems where the load fluctuates throughout the day. If the absorption of reactive power is very variable, it is advisable the use of automatic regulation in preference to fixed capacitors.

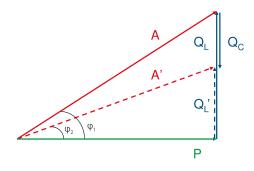
#### Power factor correction: How many?

The choice of capacitor bank to install in a system is closely depended from:

- cosφ<sub>2</sub> value that we would obtain;
- cosφ<sub>1</sub> starting value;
- · installed active power.

By the following equation:

 $Q_c = P \cdot (\tan \varphi_1 - \tan \varphi_2)$ 



Can be also written  $Q_c = k \cdot P$ 

where the parameter k is easily calculated using Table 1 (in APPENDIX).

As example if we have installed a load that absorbs an active power of 300 kW having a power factor 0.7 and we want to increase it until 0.97.

From the table 1 we find: k = 0,770. and therefore:

$$Q_c = 0.770 \cdot 300 = 231 \text{ kvar}$$

#### where:

 $Q_c$  = required capacitors reactive output (kvar); P = active power (kW);

 $Q_L$ ,  $Q_L'$  = inductive reactive output before and after the installation of the capacitor bank;

A, A'= apparent power before and after the power factor correction (kVA).

A typical example of power factor correction, sometimes not much considered but surely important, concerns the power factor correction of transformers for the distribution of energy.

It is essentially a fixed power factor correction that must compensate for the reactive power absorbed by the transformer in its no load condition (this happens often during the night). The calculation of the needed reactive output is very easy and it bases itself on this equation:

$$Q_{C} = I_{0}\% \cdot \frac{A_{N}}{100}$$

#### where

 $I_0$ % = magnetising current of the transformer  $A_N$  = apparent rated power in kVA of the transformer

If we don't have these parameters, it is convenient to use the following table.

Power	Stan	dard	Low losses			
transformer [kVA]	Oil [kvar]	Resin [kvar]	Oil [kvar]	Resin [kvar]		
10	1	1,5	-	-		
20	2	1,7	_	_		
50	4	2	-	-		
75	5	2,5	_	_		
100	5	2,5	1	2		
160	7	4	1,5	2,5		
200	7,5	5	2	2,5		
250	8	7,5	2	3		
315	10	7,5	2,5	3,5		
400	12,5	8	2,5	4		
500	15	10	3	5		
630	17,5	12,5	3	6		
800	20	15	3,5	6,5		
1000	25	17,5	3,5	7		
1250	30	20	4	7,5		
1600	35	22	4	8		
2000	40	25	4,5	8,5		
2500	50	35	5	9		
3150	60	50	6	10		

Another very important example of power factor correction concerns asynchronous three-phase motors that are individually corrected.

The reactive power likely needed is reported on following table:

Motor	power	Required reactive power [kvar]						
HP	кw	3000 rpm	1500 rpm	1000 rpm	750 rpm	500 rpm		
0,4	0,55	-	-	0,5	0,5	-		
1	0,73	0,5	0,5	0,6	0,6	-		
2	1,47	0,8	0,8	1	1	_		
3	2,21	1	1	1,2	1,6	-		
5	3,68	1,6	1,6	2	2,5	_		
7	5,15	2	2	2,5	3	-		
10	7,36	3	3	4	4	5		
15	11	4	5	5	6	6		
30	22,1	10	10	10	12	15		
50	36,8	15	20	20	25	25		
100	73,6	25	30	30	30	40		
150	110	30	40	40	50	60		
200	147	40	50	50	60	70		
250	184	50	60	60	70	80		

Be careful: the capacitor output must not be dimensioned too high for individual compensated machines where the capacitor is directly connected with the motor terminals. The capacitor placed in parallel may act as a generator for the motor which will cause serious overvoltages (self-excitation phenomena). In case of wound rotor motor the reactive power of the capacitor bank must be increased by 5%.

## Power factor correction: technical reasons

Recent energy market deregulation, along with new potential energy supplier rising, had lead to many and different type of invoicing which are not very clear in showing Power Factor up. However as energy final price is steady growing, to correct power factor is becoming more and more convenient. In most of the cases power factor improvement device prime cost is paid back in few months.

Technical-economical advantages of the installation of a capacitor bank are the following:

- Decrease of the losses in the network and on the transformers caused by the lower absorbed current.
- · Decrease of voltage drops on lines.
- · Optimisation of the system sizing.

The current I, that flows in the system, is calculated by:

$$I = \frac{P}{\sqrt{3} \cdot V \cdot \cos\varphi}$$

where

P = Active power.

V = Nominal voltage.

While cosp increases, with the same absorbed power we can obtain a reduction in the value of the current and as a consequence the losses in the network and on the transformers are reduced.

Therefore we have an important saving on the size of electrical equipment used on a system. The best system sizing has some consequence on the line voltage drop. We can easily see that looking at the following formula:

$$\Delta V = R \cdot \frac{P}{V} + X \cdot \frac{Q}{V}$$

where

P = Active power on the network (kW).

Q = Reactive power on the network (kvar)

while R is the cable resistance and X its reactance (R<<X).

The capacitor bank installation reduces Q so we have a lower voltage drop. If, for a wrong calculation of the installed capacitor bank value, the reactive part of the above equation becomes negative, instead of a reduction of the voltage drop we have an increasing of the voltage at the end of the line (Ferranti Effect) with dangerous consequence for the installed loads.

Some examples clarify the concepts set out above:

cosφ	Power loss¹ [kW]	Supplied active power <sup>2</sup> [kW]
0,5	3,2	50
0,6	2,3	60
0,7	1,6	70
0,8	1,3	80
0,9	1	90
1	0	100

1. In function of cosφ, from a copper cable 3 x 25mm² 100m long carrying 40kW at 400Vac 2. By a 100kVA transformer, in function of cosφ

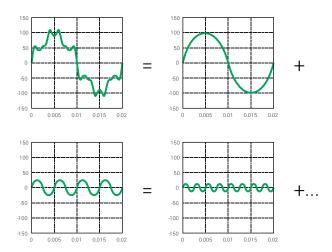
As we can see as the power factor increases we have fewer losses in the network and more active power from the same KVA. This allows us to optimise on the system sizing.

#### Power factor correction: Harmonics in the network

The distortions of the voltage and current waveforms are generated by non-linear loads (inverter, saturated transformers, rectifier, etc.) and produce the following problems:

- On the AC motors we find mechanical vibration that can reduce expected life. The increase of the losses creates overheating with consequent damaging of the insulating materials.
- In transformers they increase the copper and iron losses with possible damaging of the windings. The presence of direct voltage or current could cause the saturation of the cores with consequent increasing of the magnetising current
- The capacitors suffer from the overheating and the increasing of the voltage that reduce their life.

The waveform of the current (or voltage) generated by a nonlinear load being periodical, could be represented by the sum of many sinusoidal waves (a 50Hz component called fundamental and other components with multiple frequency of the fundamental component so called **harmonics**).

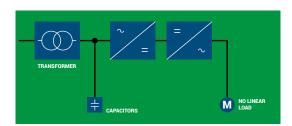


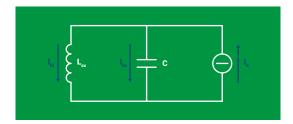
$$| = |_1 + |_2 + |_3 + ... + |_n$$

It is not advisable to install the power factor correction without considering the harmonic content of a system. This is because, even if we could manufacture capacitors that can withstand high overloads, capacitors produce an increase of harmonic content, with the negative effects just

We speak about resonance phenomena when an inductive reactance is equal to the capacitive one:

$$2\pi f L = \frac{1}{2\pi f C}$$





Ideal current generator represents motor as harmonic current components generator  $I_{h'}$  these are independent from circuit inductance, while  $L_{cc}$  is obtainable by capacitor upstream short circuit power (in general it is equal to transformer short-circuit inductance).

The resonance frequency is obtained as follows:

$$N = \sqrt{\frac{S_{cc}}{Q}} \cong \sqrt{\frac{A \cdot 100}{Q \cdot V_{cc}\%}}$$

 $S_{cc}$  = short-circuit power of the network (MVA)

Q = output of power factor correction bank (kvar)

A = rated power transformer (kVA)

V<sub>cc</sub>% = transformer short-circuit voltage

N = resonance harmonic order

In parallel resonance conditions the current and the voltage of the circuit  $\rm L_{\rm cc}$  -  $\rm C$  are heavily amplified as well as the nearby harmonic currents.

Hereinafter an example:

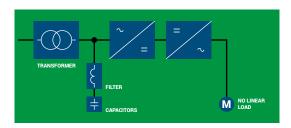
A = 630kVA (rated power transformer)

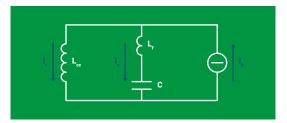
V<sub>cc</sub>% = 6 (transformer short-circuit voltage %) Q = 300kvar (output of power factor correction bank)

$$N = \sqrt{\frac{A \cdot 100}{Q \cdot V_{00}\%}} = \sqrt{\frac{630 \cdot 100}{300 \cdot 6}} \cong 6$$

The result shows that in these conditions the system transformer-capacitor bank has the parallel resonance frequency of 300Hz (6x50Hz). This means likely amplification of 5th and 7th harmonic current.

The most convenient solution to avoid this is the detuned filter, formed introducing a filter reactor in series with the capacitors, making this a more complex resonant circuit but with the desired feature of having a resonance frequency below the first existing harmonic.





With this type of solution, the parallel resonance frequency is modified from

$$f_{rp} = \frac{1}{2 \cdot \pi \cdot \sqrt{L \times C}}$$

to

$$f_{rp} = \frac{1}{2 \cdot \pi \cdot \sqrt{(L_{cc} + L_f) \times C}}$$

Normally the resonance frequency between the capacitor and the series reactance is shifted lower than 250Hz and it is generally between 135Hz and 210Hz. The lower frequencies correspond to higher harmonic loads.

The installation of a reactance in series with the capacitor bank produces a series resonance frequency:

$$f_{rs} = \frac{1}{2 \cdot \pi \cdot \sqrt{L_f \times C}}$$

If a harmonic current  $I_h$  with the same frequency of the resonance in series exists, this one will be totally absorbed by the system capacitors - reactors without any effect on the network. The realisation of a tuned passive filter is based on this simple principle.

This application is required when we want the reduction of the total distortion in current (THD) on the system:

THD = 
$$\frac{\sqrt{I_3^2 + I_5^2 + I_7^2 + ... + I_n^2}}{I_1}$$

where

I, = component at the fundamental frequency (50Hz) of the total harmonic current

I<sub>3</sub> - I<sub>5</sub> - ... = harmonic components at the multiple frequency of the fundamental (150Hz, 250Hz, 350Hz, ...)

The dimensioning of tuned/passive filters is linked to the circuit parameter:

- Impedance of the network (attenuation effect less as the short-circuit power on the network increases: in some cases could be useful to add in series with the network a reactance to increase the filtering effect).
- Presence of further loads that generate harmonics linked to other nodes on the network.
- · Capacitor types.

On this last point we have to make some considerations. It is known that the capacitors tend to decrease capacity over time: varying the capacity inevitably varies the resonance series frequency

$$f_{rs} = \frac{1}{2 \cdot \pi \cdot \sqrt{L_f \times C}}$$

and this drawback can be very dangerous because the system could lead in parallel resonance conditions. In this case, the filter does not absorb more harmonics but even amplifies them.

In order to have a constant capacity guarantee over time we need to use another type of capacitors made in bimetallized paper and oil impregnated polypropylene.

In addition to the passive absorption filter realized with capacitors and inductances is possible to eliminate the network harmonics, with another type of absorption filter: the Active Filter. The operation principle is based on the in-line injection of the same current harmonics produced by nonlinear loads, but out of phase.

# Power factor correction in the presence of a photovoltaic system in spot trading

If on electrical plant of an industrial user is added a photovoltaic system, the active power drawn from the supply is reduced because of the power supplied by the photovoltaic system and consumed by the plant (consumption).

Therefore, it changes the relationship between reactive power and active energy drawn from the network and, consequently, the power factor is lower than the same system without photovoltaic.

We must therefore pay particular attention to the power factor correction not to have any penalties for low cosp that could seriously erode the economic benefits of the photovoltaic system.

The power factor correction will be reviewed both for installed capacity, both for construction type. In fact, increasing the power factor corrector power, you will modify the resonance conditions with the MV/LV transformer which supply the system.

When the photovoltaic system has more power than the users one, or if it is possible that power is introduced to the network, the power factor corrector must also be able to run on the four quadrants. The two "standard" quadrants are related to the plant operation as a user that absorbs from the network both active and inductive reactive power, while the two quadrants related on the plant functioning as a generator, it provides the network active power, but it absorbs the inductive reactive power (quadrants of generation.

All ORTEA range of cosp electronic controllers are able to operate in four quadrants, running two different cosp targets to optimize the system economic performance.

To manage the cogeneration quadrants you can alter some parameters settings. It is advisable to enter a value equal to 1, to optimize the yield of the PFC Bank. Refer to the manuals of the controllers for more details.

To get the maximum benefit in the time allowed by the PFC Bank, we recommend to use metallized polypropylene capacitor with increased thickness.



### **APPENDIX**

**Table 1**K factor for turning active power into reactive power to achieve target power factor.

Starting power factor	Target power factor										
	0,90	0,91	0,92	0,93	0,94	0,95	0,96	0,97	0,98	0,99	1,00
0,30	2,695	2,724	2,754	2,785	2,817	2,851	2,888	2,929	2,977	3,037	3,180
0,31	2,583	2,611	2,641	2,672	2,704	2,738	2,775	2,816	2,864	2,924	3,067
0,32	2,476	2,505	2,535	2,565	2,598	2,632	2,669	2,710	2,758	2,818	2,961
0,33	2,376	2,405	2,435	2,465	2,498	2,532	2,569	2,610	2,657	2,718	2,861
0,34 0,35	2,282 2,192	2,310 2,221	2,340 2,250	2,371 2,281	2,403 2,313	2,437 2,348	2,474 2,385	2,515 2,426	2,563 2,473	2,623 2,534	2,766 2,676
0,36	2,107	2,136	2,166	2,196	2,229	2,263	2,300	2,341	2,388	2,449	2,592
0,37	2,027	2,055	2,085	2,116	2,148	2,182	2,219	2,260	2,308	2,368	2,511
0,38	1,950	1,979	2,008	2,039	2,071	2,105	2,143	2,184	2,231	2,292	2,434
0,39	1,877	1,905	1,935	1,966	1,998	2,032	2,069	2,110	2,158	2,219	2,361
0,40	1,807	1,836	1,865	1,896	1,928	1,963	2,000	2,041	2,088	2,149	2,291
0,41	1,740	1,769	1,799	1,829	1,862	1,896	1,933	1,974	2,022	2,082	2,225
0,42	1,676	1,705	1,735	1,766	1,798	1,832	1,869	1,910	1,958	2,018	2,161
0,43	1,615	1,644	1,674	1,704	1,737	1,771	1,808	1,849	1,897	1,957	2,100
0,44	1,557	1,585	1,615 1,559	1,646 1,589	1,678	1,712	1,749	1,790	1,838	1,898	2,041
0,45 0,46	1,500 1,446	1,529 1,475	1,504	1,589	1,622 1,567	1,656 1,602	1,693 1,639	1,734 1,680	1,781 1,727	1,842 1,788	1,985 1,930
0,46	1,394	1,473	1,452	1,483	1,507	1,549	1,586	1,627	1,675	1,736	1,878
0,48	1,343	1,372	1,402	1,432	1,465	1,499	1,536	1,577	1,625	1,685	1,828
0,49	1,295	1,323	1,353	1,384	1,416	1,450	1,487	1,528	1,576	1,637	1,779
0,50	1,248	1,276	1,306	1,337	1,369	1,403	1,440	1,481	1,529	1,590	1,732
0,51	1,202	1,231	1,261	1,291	1,324	1,358	1,395	1,436	1,484	1,544	1,687
0,52	1,158	1,187	1,217	1,247	1,280	1,314	1,351	1,392	1,440	1,500	1,643
0,53	1,116	1,144	1,174	1,205	1,237	1,271	1,308	1,349	1,397	1,458	1,600
0,54	1,074	1,103	1,133	1,163	1,196	1,230	1,267	1,308	1,356	1,416	1,559
0,55	1,034	1,063	1,092	1,123	1,156	1,190	1,227	1,268	1,315	1,376	1,518
0,56	0,995	1,024	1,053	1,084	1,116	1,151	1,188	1,229	1,276	1,337	1,479
0,57	0,957	0,986	1,015	1,046	1,079	1,113	1,150	1,191	1,238	1,299	1,441
0,58	0,920	0,949	0,979	1,009	1,042	1,076	1,113	1,154	1,201	1,262	1,405
0,59	0,884	0,913	0,942	0,973	1,006	1,040	1,077	1,118	1,165	1,226	1,368
0,60	0,849	0,878	0,907	0,938	0,970	1,005	1,042	1,083	1,130	1,191	1,333
0,61 0,62	0,815 0,781	0,843 0,810	0,873 0,839	0,904 0,870	0,936 0,903	0,970 0,937	1,007 0,974	1,048 1,015	1,096 1,062	1,157 1,123	1,299 1,265
0,63	0,748	0,810	0,807	0,837	0,903	0,904	0,941	0,982	1,030	1,090	1,233
0,64	0,716	0,745	0,775	0,805	0,838	0,872	0,909	0,950	0,998	1,058	1,201
0,65	0,685	0,714	0,743	0,774	0,806	0,840	0,877	0,919	0,966	1,027	1,169
0,66	0,654	0,683	0,712	0,743	0,775	0,810	0,847	0,888	0,935	0,996	1,138
0,67	0,624	0,652	0,682	0,713	0,745	0,779	0,816	0,857	0,905	0,966	1,108
0,68	0,594	0,623	0,652	0,683	0,715	0,750	0,787	0,828	0,875	0,936	1,078
0,69	0,565	0,593	0,623	0,654	0,686	0,720	0,757	0,798	0,846	0,907	1,049
0,70	0,536	0,565	0,594	0,625	0,657	0,692	0,729	0,770	0,817	0,878	1,020
0,71	0,508	0,536	0,566	0,597	0,629	0,663	0,700	0,741	0,789	0,849	0,992
0,72	0,480	0,508	0,538	0,569	0,601	0,635	0,672	0,713	0,761	0,821	0,964
0,73	0,452	0,481	0,510	0,541	0,573	0,608	0,645	0,686	0,733	0,794	0,936
0,74	0,425	0,453	0,483	0,514	0,546	0,580	0,617	0,658	0,706	0,766	0,909
0,75	0,398 0,371	0,426	0,456 0,429	0,487 0,460	0,519	0,553 0,526	0,590 0,563	0,631 0,605	0,679 0,652	0,739	0,882
0,76 0,77	0,371	0,400 0,373	0,429	0,460	0,492 0,466	0,526	0,563	0,605	0,652	0,713 0,686	0,855 0,829
0,77	0,344	0,373	0,403	0,433	0,466	0,500	0,537	0,578	0,599	0,660	0,829
0,79	0,318	0,320	0,370	0,381	0,439	0,447	0,484	0,532	0,599	0,634	0,802
0,80	0,266	0,294	0,324	0,355	0,387	0,421	0,458	0,499	0,547	0,608	0,750
0,81	0,240	0,268	0,298	0,329	0,361	0,395	0,432	0,473	0,521	0,581	0,724
0,82	0,214	0,242	0,272	0,303	0,335	0,369	0,406	0,447	0,495	0,556	0,698
0,83	0,188	0,216	0,246	0,277	0,309	0,343	0,380	0,421	0,469	0,530	0,672
0,84	0,162	0,190	0,220	0,251	0,283	0,317	0,354	0,395	0,443	0,503	0,646
0,85	0,135	0,164	0,194	0,225	0,257	0,291	0,328	0,369	0,417	0,477	0,620
0,86	0,109	0,138	0,167	0,198	0,230	0,265	0,302	0,343	0,390	0,451	0,593
0,87	0,082	0,111	0,141	0,172	0,204	0,238	0,275	0,316	0,364	0,424	0,567
0,88	0,055	0,084	0,114	0,145	0,177	0,211	0,248	0,289	0,337	0,397	0,540
0,89	0,028	0,057	0,086	0,117	0,149	0,184	0,221	0,262	0,309	0,370	0,512
0,90	-	0,029	0,058	0,089	0,121	0,156	0,193	0,234	0,281	0,342	0,484
0,91 0,92	-		0,030	0,060 0,031	0,093 0,063	0,127 0,097	0,164 0,134	0,205 0,175	0,253 0,223	0,313 0,284	0,456 0,426
0,92		-	-	0,031	0,063	0,097	0,134	0,175	0,223	0,253	0,426
0,94	-	-		-	-	0,007	0,104	0,143	0,192	0,233	0,393
-,			-	-		-	0,037	0,078	0,100	0,186	0,303

# Power factor correction of transformers MV/LV.

Power	Stan	dard	Low losses		
transformer [kVA]	Oil [kvar]	Resin [kvar]	Oil [kvar]	Resin [kvar]	
10	1	1,5	-	-	
20	2	1,7	-	_	
50	4	2	-	_	
75	5	2,5	_	_	
100	5	2,5	1	2	
160	7	4	1,5	2,5	
200	7,5	5	2	2,5	
250	8	7,5	2	3	
315	10	7,5	2,5	3,5	
400	12,5	8	2,5	4	
500	15	10	3	5	
630	17,5	12,5	3	6	
800	20	15	3,5	6,5	
1000	25	17,5	3,5	7	
1250	30	20	4	7,5	
1600	35	22	4	8	
2000	40	25	4,5	8,5	
2500	50	35	5	9	
3150	60	50	6	10	

# Power factor correction of asynchronous three-phase motors.

Attention to possible self-excitation.

Motor power		Required reactive power [kvar]				
НР	кw	3000 rpm	1500 rpm	1000 rpm	750 rpm	500 rpm
0,4	0,55	-	-	0,5	0,5	-
1	0,73	0,5	0,5	0,6	0,6	_
2	1,47	0,8	0,8	1	1	_
3	2,21	1	1	1,2	1,6	_
5	3,68	1,6	1,6	2	2,5	_
7	5,15	2	2	2,5	3	-
10	7,36	3	3	4	4	5
15	11	4	5	5	6	6
30	22,1	10	10	10	12	15
50	36,8	15	20	20	25	25
100	73,6	25	30	30	30	40
150	110	30	40	40	50	60
200	147	40	50	50	60	70
250	184	50	60	60	70	80

# Typical Power Factor of few common loads.

Type of user	cosφ	
Equipment powered by inverter	0,99	
Office appliances (computers, prin	nters, etc)	0,7
Fridges		0,8
Commercial mall		0,85
Office block		0,8
Extruders		0,4÷0,7
Resistor furnaces		1
Arc furnaces		0,8
Induction furnaces		0,85
Photovoltaic system in spot tradir	0,1÷0,9	
Incandescent lamps	1	
Discharge lamps	0,4÷0,6	
Fluorescent lamps without integra	0,5	
Fluorescent lamps with integrated	0,9÷0,93	
LED lamps without integrated PF0	0	0,3÷0,6
LED lamps with integrated PFC		0,9÷0,95
Asynchronous motor	0,2 0,55 0,72 0,8 0,85	
Mechanical workshop	0,6÷0,7	
Wooden workshop	0,7÷0,8	
Hospital	0,8	
Glassworks	0,8	





Companies are more and more sensitive to Power Quality issues because they can cause troubles and damages to equipments.

Our Power Quality solutions:

**VOLTAGE STABILISERS SAG COMPENSATOR** LV TRANSFORMERS **PFC SYSTEMS ACTIVE HARMONIC FILTERS ENERGY EFFICIENCY SMART DEVICES** 



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